
series


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## Circular diffusers 43 SF



## Description

Type 43 SF with multiple cones, positioned in one plane aligned with the ceiling.

## Finishes

Anodised aluminium in its natural colour.
Special finishes available upon request.

## General dimensions

See page 4

## 43 SF + PM

Circular diffuser with mounting bridge for fibre ducts.


## 43 SF + PMC

Circular diffuser with mounting bridge for sheet ducts.


## 43 SF + $49 \mathrm{MM}+\mathrm{PM}$ and 43 SF + 49 MM + PMC

Circular diffuser with flap damper and mounting bridge.
The volume control damper is operated through the diffuser. $H$ is the maximum height of the diffuser with the damper fully open.

| 43 SF | Series, aluminium diffuser |
| :---: | :--- |
| 49 MM | Volume control damper <br> Without indication, not incorporated |
| PM  <br> PMC Mounting bridge for fibre ducts <br> Mounting bridge for sheet ducts <br> Size From 6 to 16 according to table <br> Nom. mm. From 160 to 400 according to table |  |

## Identification

With the mounting bridge the fixing to the ceiling is quick and easy. The existing difference between exterior and neck diameters resolves space problems in certain installations.

## Quick Selection Table

## Notes:

- This selection table is based on full-scale laboratory tests according to standards ISO 5219 and ISO 5135 and 3741.
- The diffuser is placed in the centre of a square room.
- The jet is adherent, i.e. the diffuser is mounted aligned with the ceiling.
- Room height is $3 \pm 0,5 \mathrm{~m}$.
- Sound index NR is based on sound power, without room attenuation and without damper (mounting according to ISO).
- To obtain the pressure loss or sound level of diffuser 43 SF with damper, see the corresponding graph on page 13.
- Throws given correspond to a terminal velocity $\left(\mathrm{V}_{\mathrm{z}}\right)$ of $0,25 \mathrm{~m} / \mathrm{s}$ in the occupied zone.


## Symbols

$\mathrm{V}_{\mathrm{k}}=$ Effective velocity in $\mathrm{m} / \mathrm{s}$
$X=$ Throw in $m$
$\mathrm{P}_{\mathrm{t}}=$ Total pressure in Pa
NR = Noise level index in dB
$A_{k}=$ Effective area in $\mathrm{m}^{2}$

## Types

43 SF + PM
43 SF + PMC
43 SF + 49 MM + PM
43 SF + 49 MM + PMC

|  |  |  | Nominal $\varnothing$ of diffuser in mm . |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | 160 | 200 | 250 | 315 | 355 | 400 |
|  |  |  | Size |  |  |  |  |  |
| Q |  |  | 6 | 8 | 10 | 12 | 14 | 16 |
| m ${ }^{\text {\% }} \mathrm{h}$ | 1/s | $\mathrm{A}_{\mathrm{k}}$ | 0,0092 | 0,0138 | 0,0206 | 0,0312 | 0,0386 | 0,0477 |
| 100 | 27,8 | $\mathrm{V}_{\mathrm{k}}$ | 3,0 | 2,0 | 1,3 |  |  |  |
|  |  | X | 0,9 | 0,8 | 0,6 |  |  |  |
|  |  | $P_{t}$ | 3,6 | 1,6 | 0,7 |  |  |  |
|  |  | NR |  |  |  |  |  |  |
| 120 | 33,3 | $\mathrm{V}_{\mathrm{k}}$ | 3,6 | 2,4 | 1,6 |  |  |  |
|  |  | X | 1,1 | 0,9 | 0,7 |  |  |  |
|  |  | $\mathrm{P}_{\mathrm{t}}$ | 5,1 | 2,3 | 1,0 |  |  |  |
|  |  | NR | 4 |  |  |  |  |  |
| 140 | 38,9 | $\mathrm{V}_{\mathrm{k}}$ | 4,2 | 2,8 | 1,9 | 1,2 |  |  |
|  |  | X | 1,3 | 1,1 | 0,9 | 0,7 |  |  |
|  |  | $\mathrm{P}_{\mathrm{t}}$ | 7,0 | 3,1 | 1,4 | 0,6 |  |  |
|  |  | NR | 9 |  |  |  |  |  |
| 160 | 44,4 | $\mathrm{V}_{\mathrm{k}}$ | 4,8 | 3,2 | 2,2 | 1,4 | 1,2 |  |
|  |  | X | 1,5 | 1,2 | 1,0 | 0,8 | 0,7 |  |
|  |  | $\mathrm{P}_{\mathrm{t}}$ | 9,1 | 4,0 | 1,8 | 0,8 | 0,5 |  |
|  |  | NR | 14 | 4 |  |  |  |  |
| 180 | 50,0 | $\mathrm{V}_{\mathrm{k}}$ | 5,4 | 3,6 | 2,4 | 1,6 | 1,3 |  |
|  |  | X | 1,7 | 1,4 | 1,1 | 0,9 | 0,8 |  |
|  |  | $\mathrm{P}_{\mathrm{t}}$ | 11,5 | 5,1 | 2,3 | 1,0 | 0,7 |  |
|  |  | NR | 18 | 8 |  |  |  |  |
| 200 | 55,6 | $\mathrm{V}_{\mathrm{k}}$ | 6,0 | 4,0 | 2,7 | 1,8 | 1,4 | 1,2 |
|  |  | X | 1,8 | 1,5 | 1,2 | 1,0 | 0,9 | 0,8 |
|  |  | $\mathrm{P}_{\mathrm{t}}$ | 14,2 | 6,3 | 2,8 | 1,2 | 0,8 | 0,5 |
|  |  | NR | 22 | 12 | 2 |  |  |  |
| 250 | 69,4 | $\mathrm{V}_{\mathrm{k}}$ | 7,5 | 5,0 | 3,4 | 2,2 | 1,8 | 1,5 |
|  |  | X | 2,3 | 1,9 | 1,5 | 1,2 | 1,1 | 1,0 |
|  |  | $\mathrm{P}_{\mathrm{t}}$ | 22,2 | 9,9 | 4,4 | 1,9 | 1,3 | 0,8 |
|  |  | NR | 29 | 19 | 10 |  |  |  |
| 300 | 83,3 | $\mathrm{V}_{\mathrm{k}}$ | 9,1 | 6,0 | 4,0 | 2,7 | 2,2 | 1,7 |
|  |  | X | 2,8 | 2,3 | 1,8 | 1,5 | 1,3 | 1,2 |
|  |  | $\mathrm{P}_{\mathrm{t}}$ | 32,0 | 14,2 | 6,4 | 2,8 | 1,8 | 1,2 |
|  |  | NR | 36 | 26 | 16 | 6 |  |  |
| 350 | 97,2 | $\mathrm{V}_{\mathrm{k}}$ | 10,6 | 7,0 | 4,7 | 3,1 | 2,5 | 2,0 |
|  |  | X | 3,2 | 2,6 | 2,1 | 1,7 | 1,6 | 1,4 |
|  |  | $\mathrm{P}_{\mathrm{t}}$ | 43,6 | 19,4 | 8,7 | 3,8 | 2,5 | 1,6 |
|  |  | NR | 41 | 31 | 21 | 11 | 6 |  |
| 400 | 111,1 | $\mathrm{V}_{\mathrm{k}}$ |  | 8,1 | 5,4 | 3,6 | 2,9 | 2,3 |
|  |  | X |  | 3,0 | 2,5 | 2,0 | 1,8 | 1,6 |
|  |  | $\mathrm{P}_{\mathrm{t}}$ |  | 25,3 | 11,3 | 4,9 | 3,2 | 2,1 |
|  |  | NR |  | 36 | 26 | 16 | 11 | 6 |
| 450 | 125,0 | $\mathrm{V}_{\mathrm{k}}$ |  | 9,1 | 6,1 | 4,0 | 3,2 | 2,6 |
|  |  | X |  | 3,4 | 2,8 | 2,2 | 2,0 | 1,8 |
|  |  | $\mathrm{P}_{\mathrm{t}}$ |  | 32,0 | 14,4 | 6,3 | 4,1 | 2,7 |
|  |  | NR |  | 40 | 30 | 20 | 15 | 10 |
| 500 | 138,9 | $\mathrm{V}_{\mathrm{k}}$ |  | 10,1 | 6,7 | 4,5 | 3,6 | 2,9 |
|  |  | ${ }^{\text {k }}$ |  | 3,8 | 3,1 | 2,5 | 2,2 | 2,0 |
|  |  | $\mathrm{P}_{\mathrm{t}}$ |  | 39,5 | 17,7 | 7,7 | 5,0 | 3,3 |
|  |  | NR |  | 44 | 34 | 24 | 19 | 13 |
| 600 | 166,7 | V |  | 12,1 | 8,1 | 5,3 | 4,3 | 3,5 |
|  |  | X |  | 4,5 | 3,7 | 3,0 | 2,7 | 2,4 |
|  |  | $\mathrm{P}_{\mathrm{t}}$ |  | 56,9 | 25,5 | 11,1 | 7,3 | 4,8 |
|  |  | NR |  | 50 | 40 | 30 | 25 | 20 |
| 700 | 194,4 | $\mathrm{V}_{\mathrm{k}}$ |  |  | 9,4 | 6,2 | 5,0 | 4,1 |
|  |  | X |  |  | 4,3 | 3,5 | 3,1 | 2,8 |
|  |  | $\mathrm{P}_{\mathrm{t}}$ |  |  | 34,7 | 15,1 | 9,9 | 6,5 |
|  |  | NR |  |  | 46 | 35 | 30 | 25 |
| 800 | 222,2 | $\mathrm{V}_{\mathrm{k}}$ |  |  | 10,8 | 7,1 | 5,8 | 4,7 |
|  |  | X |  |  | 4,9 | 4,0 | 3,6 | 3,2 |
|  |  | $\mathrm{P}_{\mathrm{t}}$ |  |  | 45,4 | 19,8 | 12,9 | 8,5 |
|  |  | NR |  |  | 50 | 40 | 35 | 30 |
| 900 | 250,0 |  |  |  | 12,1 | 8,0 | 6,5 | 5,2 |
|  |  | X |  |  | 5,5 | 4,5 | 4,0 | 3,6 |
|  |  | $\mathrm{P}_{\mathrm{t}}$ |  |  | 57,4 | 25,0 | 16,4 | 10,7 |
|  |  | NR |  |  | 54 | 44 | 39 | 34 |
| 1000 | 277,8 | $\mathrm{V}_{\mathrm{k}}$ |  |  |  | 8,9 | 7,2 | 5,8 |
|  |  | X |  |  |  | 5,0 | 4,5 | 4,0 |
|  |  | $\mathrm{P}_{\mathrm{t}}$ |  |  |  | 30,9 | 20,2 | 13,2 |
|  |  | NR |  |  |  | 48 | 43 | 37 |
| 1200 | 333,3 | $\mathrm{V}_{\mathrm{k}}$ |  |  |  | 10,7 | 8,6 | 7,0 |
|  |  | X |  |  |  | 6,0 | 5,4 | 4,8 |
|  |  | $\mathrm{P}_{\mathrm{t}}$ |  |  |  | 44,5 | 29,1 | 19,0 |
|  |  | NR |  |  |  | 54 | 49 | 44 |
| 1400 | 388,9 | $\mathrm{V}_{\mathrm{k}}$ |  |  |  | 12,5 | 10,1 | 8,2 |
|  |  | X |  |  |  | 7,0 | 6,3 | 5,7 |
|  |  | $\mathrm{P}_{\mathrm{t}}$ |  |  |  | 60,6 | 39,6 | 25,9 |
|  |  | NR |  |  |  | 60 | 54 | 49 |
| 1600 | 444,4 | $\mathrm{V}_{\mathrm{k}}$ |  |  |  |  | 11,5 | 9,3 |
|  |  | X |  |  |  |  | 7,2 | 6,5 |
|  |  | $\mathrm{P}_{\mathrm{t}}$ |  |  |  |  | 51,7 | 33,9 |
|  |  | NR |  |  |  |  | 59 | 54 |

## General information

## General dimensions

| Diffuser <br> size | Dimensions in mm |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $\varnothing \mathrm{N}$ | $\varnothing \mathrm{A}$ | $\varnothing \mathrm{B}$ | $\varnothing \mathrm{C}$ | H |  |
| 6 | 160 | 159 | 213 | 247 | 132 |  |
| 8 | 200 | 199 | 264 | 287 | 152 |  |
| 10 | 250 | 249 | 315 | 337 | 177 |  |
| 12 | 315 | 314 | 366 | 402 | 209 |  |
| 14 | 355 | 354 | 417 | 442 | 229 |  |
| 16 | 400 | 399 | 462 | 487 | 252 |  |

## Example of selection

## Requirements

Air flow rate: $\qquad$ $300 \mathrm{~m}^{3} / \mathrm{h}$
Throw: $\qquad$
$\qquad$ 1,3 to $1,6 \mathrm{~m}$
Sound level: below 20 NR
Application: $\qquad$ Offices
Required pressure loss: $\qquad$ below 10 Pa

## Symbols

$\varnothing \mathrm{N}=$ Duct diameter in mm
$\varnothing \mathrm{A}=$ Exterior neck diameter of diffuser in mm
$\varnothing B=$ Diameter of opening in ceiling in mm
$\varnothing C=$ Total exterior diameter of diffuser in mm
$\mathrm{H}=$ Maximum height of the diffuser with the volume control damper fully open

## Solution

With the selection table for diffusers type 43 SF and following the general criterion that for comfort installations the recommended discharge velocity for this type of diffusers lies between 2 and $3 \mathrm{~m} / \mathrm{s}$, we obtain:

Q (Air flow rate) $\qquad$ $300 \mathrm{~m}^{3} / \mathrm{h}$
$\mathrm{V}_{\mathrm{k}}$ (Effective velocity) $2,7 \mathrm{~m} / \mathrm{s}$
X (Throw) $1,5 \mathrm{~m}$
$\mathrm{P}_{\mathrm{t}}$ (Pressure loss) $\quad 2,8 \mathrm{~Pa}$
NR (Sound level) $\qquad$
Diffuser 43 SF + PM or PMC size 12 (Ø 315 mm).
With optional delivery of damper 49 MM Observing the results, the data obtained fulfil the requirements of the project.

## Throw correction factor for distance of diffuser to ceiling ( $C_{h}$ )

For adherent jets, i.e. diffuser aligned with ceiling:

$$
C_{h}=1
$$

For free jets, with the diffuser separated from the ceiling:

$$
C_{h}=1,4
$$

The corrected throw $\left(\mathrm{X}_{\mathrm{c}}\right)$ is obtained by multiplying the throw $(X)$ by the throw correction factor $\left(\mathrm{C}_{\mathrm{h}}\right)$.

$$
X_{c}=X \cdot C_{h}
$$

## Nützliche Hinweise

## 1. Maximum distance of diffuser to ceiling.

To obtain an adhering jet with cold air, it is advisable not to exceed the distance of the diffuser with respect to the ceiling (h max.) and the temperature difference $\Delta t$ (difference between room and supply air temperature) according to the following table.

| $\Delta \mathrm{t}$ | $\left({ }^{\circ} \mathrm{C}\right)$ | 0 | 6 | 9 | 12 |
| :---: | :---: | :---: | :---: | :---: | :---: |
| $\mathrm{~h} \max$ | $(\mathrm{~m})$ | 0,15 | 0,09 | 0,06 | 0,04 |

## 2. Minimum recommended velocity in occupied zone, $\mathbf{V}_{\mathbf{z}}$

 Due to the difference in the temperature of the air in the room with respect to the cold supply air, the following velocities $\mathrm{V}_{\mathrm{z}}$ are recommended:| $\Delta \mathrm{t}$ | $\left({ }^{\circ} \mathrm{C}\right)$ | 0 | 6 | 9 | 12 |
| :---: | :---: | :---: | :---: | :---: | :---: |
| $\mathrm{~V}_{\mathrm{z}}$ | $(\mathrm{m} / \mathrm{s})$ | 0,23 | 0,19 | 0,15 | 0,15 |

## 3. Flow rate measurement

The air flow rate $\left(q_{v}\right)$ is obtained from the product of the effective area of the diffuser $\left(\mathrm{A}_{k}\right)$ and its effective velocity $\left(\mathrm{V}_{\mathrm{k}}\right)$, measured with a probe type ALNOR 2220 or 6070P.

$$
\mathrm{q}_{\mathrm{r}}\left(\mathrm{~m}^{3} / \mathrm{h}\right)=\mathrm{A}_{k}\left(\mathrm{~m}_{2}\right) \cdot \mathrm{V}_{k}(\mathrm{~m} / \mathrm{s}) \cdot 3600
$$

If a hot-wire anemometer is used (e.g. type TSIVELOCICALC), the velocity obtained should be multiplied by 1,33 .


## Measurement with Alnor probe

## 4. Induction effect

It is also possible to obtain the air flow rate induced in the room from the so-called induction factor ( $q_{x} / q_{0}$ ) which is determined by the parameters $X_{c}$ in $m$ (corrected throw) and the effective discharge area $A_{k}$ in $\mathrm{m}^{2}$, according to the following figure.


## 5. Technical data on volume control damper 49 MM

The volume control damper 49 MM modifies the values of sound level and pressure loss given in the selection table.

Hereafter, and in the corresponding graph sound levels and total pressure losses $(\Delta \mathrm{Pt})$ are presented for the diffuser including the volume control damper as a function of the parameters Vk (effective velocity) and percentage of opening of the damper.


A correction factor should be applied to the sound level as a function of the nominal diameter of the diffuser according to the following table.

| $\varnothing$ | 160 | 200 | 250 | 315 | 355 | 400 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| NR | -2 | 0 | +3 | +4 | +5 | +6 |



## Circular diffusers 44 SF and 45 SF



## 44 SF

Circular diffuser with core adjustable in height.


## 44 SF + PM

Circular diffuser with mounting bridge for sheet ducts.

## 44 SF + 49 ML + PM

Circular diffuser with flap damper and mounting bridge. The volume control damper is operated through the diffuser.


## 44 SF + 49 MO

(Sizes 4 to 12, Ø 100 to 315)
Circular diffuser with volume control damper with blades connected to the central axis. The volume control damper is operated through the diffuser.

## 44 SF + 49 MO

(Sizes 14 to 24, Ø 355 to 630)
Circular diffuser with volume control damper with multiple blades connected to the central axis. The volume control damper is operated through the diffuser.

## Identification

This diffuser type is ideal for application in high ceilings. By manually rotating the central cone a good air distribution can be obtained.
The volume control damper can easily be operated by removing the central part of the diffuser.

## Possible combinations of diffuser 44 SF with volume control dampers and mounting systems.

| SIZE | NOMINAL $\varnothing$ | DAMPER |  |  | MOUNTING SYSTEM |  |  | DAMPER + MOUNTING SYSTEM |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | 49 ML | 49 MM | 49 MO | PM | PMC | SM | $49 \mathrm{ML}+\mathrm{PM}$ | $49 \mathrm{ML}+\mathrm{PMC}$ | $49 \mathrm{ML}+\mathrm{SM}$ | $49 \mathrm{MO}+\mathrm{SM}$ |
| 4 | 100 |  |  | O |  |  | O |  |  |  | O |
| 6 | 160 |  |  | $\bigcirc$ | $\bigcirc$ | O | ) | $0$ | O | O | , |
| 8 | 200 | O |  | O | $\bigcirc$ | O | O | O | O | O | O |
| 10 | 250 | - |  | O | ) | O | $\bigcirc$ | O | O | O | O |
| 12 | 315 | ) |  | ) | ) | 0 | ) | O | O | O | ) |
| 14 | 355 | ) |  | ) |  | 0 | O | O | O | O | O |
| 16 | 400 | O |  | ) | ) | O |  | O | O |  |  |
| 18 | 450 |  |  | O |  |  |  |  |  |  |  |
| 21 | 500 |  |  | ) |  |  |  |  |  |  |  |
| 24 | 630 |  |  | $\bigcirc$ |  |  |  |  |  |  |  |



## Description

Type 45 SF with removable core, adjustable in two fixed positions.

## Finishes

Anodised aluminium in its natural colour.
Special finishes available upon request.

## General dimensions

See page 11.


## 45 SF

Circular diffuser with removable core, adjustable in two fixed positions.


## 45 SF + 49 MM + PM

Circular diffuser with blade damper and mounting bridge. The volume control damper is operated through the diffuser.


## 45 SF + 49 MO

(Sizes 4 to 12, Ø 100 to 315)
Circular diffuser with volume control damper with blades connected to the central axis. The volume control damper is operated through the diffuser.


| 45 SF | Series, aluminium diffuser |
| :---: | :--- |
| 49 ML | Without indication, not incorporated <br> Volume control damper with blades <br> Volume control damper with multiple blades |
| PM <br> PMC <br> SM | Without indication, not incorporated <br> Mounting bridge for fibre ducts <br> Mounting bridge for sheet ducts <br> Mounting system |
| Size | From 4 to 24 according to table |
| Nom. $\varnothing$ mm. | From 100 to 630 according to table |

## 45 SF + 49 MO

(Sizes 14 to 24, Ø 355 to 630)
Circular diffuser with volume control damper with multiple blades connected to the central axis. The volume control damper is operated through the diffuser.

## Identification

This type of diffuser is ideal for installations with hot or cold air. For cold air the cones are placed in the lower position, while for hot air they are located in the upper position. The core can easily be removed by pressing the fixing clips.
The volume control damper can easily be operated by removing the central part of the diffuser.

## Mögliche Kombinationen der Auslässe 45 SF mit Drosselklappe und Montagesystem

| SIZE | NOMINAL <br> $\varnothing$ | DAMPER |  |  | MOUNTING SYSTEM |  |  | DAMPER + MOUNTING SYSTEM |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | 49 ML | 49 MM | 49 MO | PM | PMC | SM | $49 \mathrm{ML}+\mathrm{PM}$ | $49 \mathrm{ML}+$ PMC | $49 \mathrm{ML}+\mathrm{SM}$ | $49 \mathrm{MO}+\mathrm{SM}$ |
| 4 | 100 |  |  | O |  |  | $\bigcirc$ |  |  |  | O |
| 6 | 160 | $\bigcirc$ |  | $\bigcirc$ | $\bigcirc$ | $\bigcirc$ | $\bigcirc$ | O | O | O | O |
| 8 | 200 | O |  | O | $\bigcirc$ | $\bigcirc$ | $\bigcirc$ | O | O | O | $\bigcirc$ |
| 10 | 250 | O |  | 0 | $\bigcirc$ | O | $\bigcirc$ | O | O | O | $\bigcirc$ |
| 12 | 315 | O |  | $\bigcirc$ | 0 | O | $\bigcirc$ | O | 0 | O | O |
| 14 | 355 | O |  | $\bigcirc$ | O | O | $\bigcirc$ | O | O | O | O |
| 16 | 400 | O |  | O | O | $\bigcirc$ |  | O | O |  |  |
| 18 | 450 |  |  | $\bigcirc$ |  |  |  |  |  |  |  |
| 21 | 500 |  |  | O |  |  |  |  |  |  |  |
| 24 | 630 |  |  | $\bigcirc$ |  |  |  |  |  |  |  |

## Quick Selection Table (diffusers type 44 SF and 45 SF)

| Q |  |  | Nominal $\varnothing$ of diffuser in mm. |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | 100 | 160 | 200 | 250 | 315 | $355$ | 400 | 450 | 500 | 630 |
|  |  |  | 4 | $6$ | $8$ |  |  |  |  |  |  |  |
| ( $\mathrm{m}^{3 / \mathrm{h}}$ ) | (1/s) | AK | 0,0051 | 0,0144 | 0,0225 | 0,0338 | 0,0512 | 0,0679 | 0,0898 | 0,1029 | 0,1285 | 0,2079 |
| 100 | 27,8 | ${ }^{V}{ }^{\text {k }}$ | 5,4 | 1,9 | 1,2 |  |  |  |  |  |  |  |
|  |  | X | 0,9 | 0,5 | 0,4 |  |  |  |  |  |  |  |
|  |  | $\begin{aligned} & P t \\ & N R \end{aligned}$ | 17,8 24 | 2,2 |  |  |  |  |  |  |  |  |
| 160 | 44,4 | ${ }^{\mathrm{V}} \mathrm{k}$ | 8,7 | 3,1 | ${ }^{2,0}$ | 1,3 |  |  |  |  |  |  |
|  |  | $\begin{aligned} & x \\ & P_{t} \end{aligned}$ | 1,4 45,6 | 0,8 5,7 | 0,7 2,3 | 0,5 1,0 |  |  |  |  |  |  |
|  |  | NR | 39 | 9 |  |  |  |  |  |  |  |  |
| 200 | 55,6 | Vk | 10,9 | 3,9 | 2,5 | 1,6 | 1,1 |  |  |  |  |  |
|  |  | X | 1,8 | 1,0 | ${ }_{3}$, 8 | 0,7 | 0,6 |  |  |  |  |  |
|  |  | Pt NR | 71,2 46 | 8,9 16 |  |  |  |  |  |  |  |  |
| 300 | 83,3 | $\mathrm{V}^{\mathrm{k}}$ |  | 5,8 1,6 | 3,7 1,3 | 2,5 1,0 | 1,6 0,8 | 1,2 0,7 |  |  |  |  |
|  |  | $\begin{aligned} & X \\ & P_{t} \end{aligned}$ |  | 20, 20 | 1,2 8,2 | 1,0 3,6 | 0,8 1,6 | 0,9 |  |  |  |  |
|  |  | NR |  | 30 | 17 | 5 |  |  |  |  |  |  |
| 400 | 111,1 | $\mathrm{V}^{\mathrm{k}}$ |  | 7,7 | 4,9 1 | 3,3 | 2,2 | 1,6 | 1,2 |  |  |  |
|  |  | $\stackrel{X}{\mathrm{P}}$ |  | 2,1 35,7 | 14,6 | 1,4 6,5 | 1,1 | 1,0 1,6 | -8,9 |  |  |  |
|  |  | NR |  | 39 | 26 | 15 |  |  |  |  |  |  |
| 500 | 138,9 | Vk |  | 9,6 | 6,2 | 4,1 | 2,7 | 2,0 | 1,5 | 1,3 |  |  |
|  |  | $\underset{P t}{X}$ |  | 2, ${ }_{5}{ }^{2} 8$ | 2, ${ }^{2} 9$ | 1,7 101 | 1,4 4 4 | 1,2 2 | 1,1 1,4 | 1,0 1,1 |  |  |
|  |  | N R |  | 46 | +3319 | 22 |  |  |  |  |  |  |
| 600 | 166,7 | $\checkmark \mathrm{k}$ |  |  | 7,4 | 4,9 | 3,3 | 2,5 | 1,9 | 1 ,6 | 1,3 |  |
|  |  | $\begin{aligned} & x \\ & P_{t} \end{aligned}$ |  |  | 2,59 | 2,1 14 | 1,7 <br> 6 | 1,4 | 1,3 2 | 1,2 | 1,1 1,0 |  |
|  |  | Pt NR |  |  | 32,9 39 | 14,6 28 | 6,4 16 | 3, 8 |  |  |  |  |
| 700 | 194,4 | $\mathrm{V}^{\mathrm{k}}$ |  |  | 8,6 2,9 |  |  |  |  | 1,9 | 1,5 | 0,9 |
|  |  | ${ }_{P}^{\text {Pt }}$ |  |  | 44,8 | 2, 19,9 | 1,7 8,7 | 1,7 4,9 | 1,5 2,8 | 1,4 2,1 | 1,2 1,4 | 1,0 |
|  |  | NR |  |  | 44 | 33 | 21 | 13 | 5 |  |  |  |
| 800 | 222,2 | $\checkmark \mathrm{k}$ |  |  | 9,9 | 6,6 | 4,3 | 3,3 | 2,5 | 2,2 | 1,7 | 1,1 |
|  |  | X |  |  | 3,4 | 2,7 | 2,2 | 1,9 | 1,7 | 1,6 | 1,4 | 1,1 |
|  |  | Pt $\mathrm{N} R$ |  |  | 58,5 49 | 25,9 37 | 11,3 25 | 6,4 17 | 3,7 | 2,8 | 1,8 | 0,7 |
| 900 | 250,0 | $\checkmark \mathrm{k}$ |  |  |  | 7,4 | 4,9 | 3,7 | 2,8 | 2,4 | 1,9 | 1,2 |
|  |  | ${ }^{\times}$ |  |  |  | 3,18 | 2,5 | 2,2 | 1,9 | 1,8 | 1,6 2,3 | 1,2 |
|  |  | Pt NR |  |  |  | 32,8 41 | 14,3 29 | 8,1 21 | 4,7 13 | 3,5 |  |  |
| 1000 | 277,8 | $\checkmark \mathrm{k}$ |  |  |  | 8,2 | 5,4 | 4,1 | 3,1 | 2,7 | 2,2 | 1,3 |
|  |  | X |  |  |  | 3,4 | 2,8 | 2,4 | 2,1 | 2,0 | 1,8 | 1,4 |
|  |  | Pt |  |  |  | 40,5 44 | 17,7 | 10,0 | 5,7 | 4,4 | 2,8 | 1,1 |
| 1200 | 333,3 |  |  |  |  |  |  |  |  |  |  |  |
|  |  | $\checkmark \mathrm{k}$ |  |  |  | 9,9 | 6,5 | 4,9 | 3,7 | 3 ,2 | 2,6 | 1,6 |
|  |  | $\begin{aligned} & X \\ & P \mathrm{P} \end{aligned}$ |  |  |  | 4,1 58,4 | 3,3 25,4 | 2,9 14,5 | 2,5 8,3 | 2,4 6,3 | 2,1 4,0 | 1,7 1,5 |
|  |  | NR |  |  |  | 50 | 38 3 | 30 | 22 | 18 | 12 |  |
| 1400 | 388,9 | $\mathrm{V}^{\mathrm{k}}$ |  |  |  |  | 7,6 | 5,7 | 4,3 | 3,8 | 3,0 | 1,9 |
|  |  | X |  |  |  |  | 3,9 | 3,4 | 2,9 | 2,7 | 2,5 | 1,9 |
|  |  | $\mathrm{Pt}$ |  |  |  |  | 34,6 43 | 19,7 | 11,3 | 8,6 23 | 5,5 | 2,1 |
| 1600 | 444,4 |  |  |  |  |  | 8,7 |  |  | 4,3 | 3,5 |  |
|  |  | X |  |  |  |  | 4,5 | 3,9 | 3,4 | 3,1 | 2,8 | 2,2 |
|  |  | Pt NR |  |  |  |  | 45,2 | 25,7 | 14,7 | 11,2 | 7,2 | 2,7 |
| 1800 | 500,0 | V k | $V_{k}=$ Effective velocity in $\mathrm{m} / \mathrm{s}$ |  |  |  | 9,8 | 7,4 | 5,6 | 4,9 | 3,9 | 2,4 |
|  |  | X | $X=$ Throw in $m$ |  |  |  | 5,0 | 4,3 | 3, 8 | 3,5 | 3,2 | 2,5 |
|  |  | Pt |  |  |  |  | 57,2 | 32,5 | 18,6 | 14.2 | 9,1 | 3,5 |
| 2000 | 555,6 | NR | $N R=$ Noise level index in dB |  |  |  | 10.9 | 8.2 | $\frac{36}{6,2}$ | 5.4 | 4.3 | 2,7 |
|  |  | X |  |  |  |  | 5,6 | 4,8 | 4,2 | 3,9 | 3,5 | 2,8 |
|  |  | Pt |  |  |  |  | 70,6 | 40,2 | 23,0 | 17,5 | 11,2 | 4,3 |
|  |  | NR |  |  |  |  | 55 | 47 | 39 | 35 | 29 | 15 |
| 2500 | 694,4 |  |  |  |  |  |  |  | 7,7 | 6,7 | 5,4 |  |
|  |  | X |  |  |  |  |  | 6,0 | 5,3 | 4,9 | 4,4 | 3,5 |
|  |  | Pt NR |  |  |  |  |  | 62,8 54 | 35,9 46 | 27,3 42 | 17,5 36 | 6,7 22 |
| 3000 | 833,3 | V k | Notes: |  |  |  |  |  |  |  |  |  |
|  |  | X |  |  |  |  |  |  | 6,3 | 5,9 | 5,3 | 4,1 |
|  |  | $\begin{gathered} P t \\ N R \end{gathered}$ |  |  |  |  |  |  | 51,7 52 | 39,4 48 | 25,2 42 | 9,6 28 |
| 3500 | 972,2 | ${ }^{\text {V }}$ k |  |  |  |  |  |  |  | 9,4 | 7,6 | 4,7 |
|  |  | X Pt | This selection table is based on full-scale laboratory tests according to standards ISO 5219 and ISO 5135 and 3741. |  |  |  |  |  |  | 6,9 53,6 | 6,1 34 | 4,8 13,1 |
|  |  | NR |  |  |  |  |  |  |  | 53,6 53 | 34,3 47 | 13,1 33 |
| 4000 | 1111,1 | Vk |  |  |  |  |  |  |  | 10,8 | 8 8,6 |  |
|  |  | X Pt |  |  |  |  |  |  |  | 7,9 70,0 | 7,0 44,9 | 5,5 17,1 |
|  |  | N R | The jet is adherent, i.e. the diffuser is mounted aligned with the ceiling. |  |  |  |  |  |  | 58 | 51 | 37 |
| 4500 | 1250,0 | $\mathrm{V}^{\mathrm{k}}$ | The diffuser tested was of type 44 SF with the cones in intermediate position. |  |  |  |  |  |  |  | 9,7 |  |
|  |  | $\stackrel{\mathrm{X}}{\mathrm{P}} \mathrm{t}$ |  |  |  |  |  |  |  |  | 7,98 | 6,2 21,7 |
|  |  | NR | Room height is $3 \pm 0,5 \mathrm{~m}$. |  |  |  |  |  |  |  | 55 | 41 |
| 5000 | 1388,9 | ${ }^{\mathrm{V}}{ }^{\mathrm{k}}$ |  |  |  |  |  |  |  |  | 10,8 | 6,7 |
|  |  | $\begin{aligned} & X \\ & P \mathrm{t} \end{aligned}$ | Sound index NR is based on sound power, without room attenuation and without |  |  |  |  |  |  |  | 8,81 70,1 | 2,9 268 |
|  |  | N R |  |  |  |  |  |  |  |  | 59 | 45 |
| 6000 | 1666,7 | Vk |  |  |  |  |  |  |  |  |  |  |
|  |  | $\underset{\mathrm{Pt}}{\mathrm{X}}$ | Throws given correspond to a terminal velocity (Vz) of $0,25 \mathrm{~m} / \mathrm{s}$ in the occupied zone. |  |  |  |  |  |  |  |  | 8,3 386 |
|  |  | NR |  |  |  |  |  |  |  |  |  | 51 51 |
| 7000 | 1944,4 |  | To obtain the pressure loss or sound level of diffusers 44 SF and 45 SF with damper, see the corresponding graph on page 13. |  |  |  |  |  |  |  |  | 9,4 |
|  |  | X |  |  |  |  |  |  |  |  |  | 9,7 |
|  |  | $\mathrm{N}^{\mathrm{P}} \mathrm{R}$ |  |  |  |  |  |  |  |  |  | 52,5 56 |
| 8000 | 2222,2 |  |  |  |  |  |  |  |  |  |  |  |
|  |  | X |  |  |  |  |  |  |  |  |  | 11,0 |
|  |  | $\begin{aligned} & \mathrm{Pt} \\ & \mathrm{NR} \end{aligned}$ |  |  |  |  |  |  |  |  |  | 68,6 60 |

## General information

## General dimensions

| Diffusersize | Dimensions in mm |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $\varnothing$ N | $\varnothing$ A | $\varnothing$ B | $\varnothing$ C | D | E | F | G | H | 1 |
| 4 | 100 | 099 | 220 | 240 | 15 | 74 | 0 | 12 | - |  |
| 6 | 160 | 159 | 286 | 316 | 20 | 80 | 6 | 18 | 160 | 72 |
| 8 | 200 | 199 | 385 | 415 | 20 | 92 | 8 | 20 | 192 | 92 |
| 10 | 250 | 249 | 468 | 498 | 20 | 105 | 10 | 22 | 230 | 92 |
| 12 | 315 | 314 | 566 | 606 | 25 | 119 | 6 | 28 | 277 | 92 |
| 14 | 355 | 354 | 664 | 714 | 30 | 134 | 12 | 34 | 312 | 137 |
| 16 | 400 | 399 | 754 | 814 | 35 | 145 | 12 | 34 | 345 | 137 |
| 18 | 450 | 449 | 850 | 920 | 40 | 158 | 20 | 42 | - |  |
| 21 | 500 | 499 | 985 | 1055 | 40 | 180 | 20 | 42 | - |  |
| 24 | 630 | 629 | 1108 | 1188 | 45 | 196 | 25 | 47 | - |  |

## Example of selection

## Requirements

| Air flow rate | 2000 m³/h |
| :---: | :---: |
| Throw | 3 to 4 m |
| Sound level | below 30 NR |
| Application | Public building hall |
| Required pressure loss | below 15 Pa | 3 to

Sound level
$\qquad$ Public building hall
Required pressure loss below 15 Pa

## Symbols

$\varnothing \mathrm{N}=$ Duct diameter in mm
$\varnothing A=$ Exterior neck diameter of diffuser in mm
$\varnothing B=$ Diameter of opening in ceiling in mm
$\varnothing C=$ Total exterior diameter of diffuser in mm
$\mathrm{D}=$ Width of the exterior ring of the diffuser in mm
$E=$ Height of the diffuser in mm
F = Distance from core in lower position to the reference level in mm
$G=$ Distance from core in upper position to the reference level in mm
$\mathrm{H}=$ Maximum height of the diffuser with the volume control damper fully open
I = Height of mounting bridge

## Solution:

With the selection table for diffusers type 44 SF and 45 SF and following the general criterion that for comfort installations the recommended discharge velocity for this type of diffusers lies between 2,5 and $4,5 \mathrm{~m} / \mathrm{s}$, we obtain:

Q (Air flow rate) $\qquad$ $2000 \mathrm{~m}^{3} / \mathrm{h}$
$\mathrm{V}_{\mathrm{k}}$ (Effective velocity) $4,3 \mathrm{~m} / \mathrm{s}$
X (Throw) $\qquad$ $3,5 \mathrm{~m}$
$P_{t}$ (Pressure loss) $\qquad$ $11,2 \mathrm{~Pa}$
NR (Sound level) $\qquad$ 29

Diffuser 44 SF or 45 SF size 21 (Ø 500 mm )
With optional delivery of damper and mounting system.
Observing the results, the data obtained fulfil the requirements of the project.

## Throw correction factor for distance of diffuser to ceiling ( $\mathrm{C}_{\mathrm{h}}$ )

For adherent jets, i.e. diffuser aligned with ceiling:

$$
C_{h}=1
$$

For free jets, with the diffuser separated from the ceiling:

$$
C_{h}=1,4
$$

The corrected throw $\left(\mathrm{X}_{c}\right)$ is obtained by multiplying the throw $(X)$ by the throw correction factor $\left(\mathrm{C}_{\mathrm{h}}\right)$.

$$
X_{c}=X \cdot C_{h}
$$

## Useful recommendations

## 1. Core position

1.a. In the 44 SF series the core is adjusted by rotation, allowing distribution of the air in different directions. In the upper position, with the core " G " mm above the reference level (i.e. the exterior ring) a vertical flow is obtained. In intermediate position, with the core aligned with the exterior ring, a horizontal flow is achieved, with data according to the selection table. In lower position, with the central part 20 mm below the exterior ring, a
horizontal distribution is obtained, resulting in a 20\% increase in throw, the same pressure loss and a 4 dB lower noise level.
1.b. In the 45 SF series the central part can be placed in two fixed positions. In the upper position a vertical flow is obtained, while in the lower position a horizontal flow is achieved with a throw equal to the 44 SF series, a $20 \%$ higher pressure loss and a 2 dB higher noise level.


## 2. Maximum distance of diffuser to ceiling.

To obtain an adhering jet with cold air, it is advisable not to exceed the distance of the diffuser with respect to the ceiling ( h max.) and the temperature difference $\Delta \mathrm{t}$ (difference between room and supply air temperature) according to the following table.

| $\Delta^{\mathrm{t}}$ | $\left({ }^{\circ} \mathrm{C}\right)$ | 0 | 6 | 9 | 12 |
| :---: | :---: | :---: | :---: | :---: | :---: |
| $\mathrm{~h} \max$ | $(\mathrm{~m})$ | 0,70 | 0,40 | 0,27 | 0,20 |

## 3. Minimum recommended velocity in occupied zone, $\mathrm{V}_{\mathbf{z}}$

Due to the difference in the temperature of the air in the room with respect to the cold supply air, the following velocities $\mathrm{V}_{\mathrm{z}}$ are recommended:

| $\Delta \mathrm{t}$ | $\left({ }^{\circ} \mathrm{C}\right)$ | 0 | 6 | 9 | 12 |
| :---: | :---: | :---: | :---: | :---: | :---: |
| $\mathrm{~V}_{\mathrm{z}}$ | $(\mathrm{m} / \mathrm{s})$ | 0,23 | 0,19 | 0,15 | 0,15 |

## 4. Flow rate measurement

The air flow rate ( $\mathrm{q}_{\mathrm{v}}$ ) is obtained from the product of the effective area of the diffuser ( $A_{k}$ ) and its effective velocity $\left(\mathrm{V}_{\mathrm{k}}\right)$, measured with a probe type ALNOR 2220 or 6070P and with the cones in intermediate position:

$$
\mathrm{q}_{\mathrm{v}}\left(\mathrm{~m}^{3} / \mathrm{h}\right)=\mathrm{A}_{\mathrm{k}}\left(\mathrm{~m}^{2}\right) \cdot \mathrm{V}_{\mathrm{k}}(\mathrm{~m} / \mathrm{s}) \cdot 3600
$$

If a hot-wire anemometer is used (e.g. type TSIVELOCICALC), the velocity obtained should be multiplied by 1,33 .

## Measurement with Alnor probe



## 5. Induction effect

It is also possible to obtain the air flow rate induced in the room from the so-called induction factor ( $\mathrm{q}_{\mathrm{x}} / \mathrm{q}_{\mathrm{o}}$ ) which is determined by the parameters $X_{c}$ in $m$ (corrected throw) and the effective discharge area $A$ in $\mathrm{m}^{2}$, according to the following figure.


## 6. Volume control dampers $49 \mathrm{MM}, 49 \mathrm{ML}$ and 49 MO

## Technical data

The volume control dampers modify the values of sound level and pressure loss given in the selection table. Hereafter, and in the corresponding graphs sound levels and total pressure losses $\left(\Delta \mathrm{P}_{\mathrm{t}}\right)$ are presented for the diffuser including the volume control damper as a function of the parameters $\mathrm{V}_{\mathrm{k}}$ (effective velocity) and position of the damper.
6.a. Dampers 49 MM and 49 ML (position in degrees)


A correction factor should be applied to the sound level as a function of the nominal diameter of the diffuser according to the following table.

| $\varnothing$ | 160 | 200 | 250 | 315 | 355 | 400 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| NR | -2 | 0 | +3 | +4 | +5 | +6 |


6.b. Damper 49 MO (position in degrees)


A correction factor should be applied to the sound level as a function of the nominal diameter of the diffuser according to the following table:

| $\varnothing$ | 100 | 160 | 200 | 250 | 315 |
| :---: | :---: | :---: | :---: | :---: | :---: |
| NR | -5 | -2 | -1 | 0 | +1 |


| $\varnothing$ | 355 | 400 | 450 | 500 | 630 |
| :---: | ---: | ---: | :---: | :---: | :---: |
| NR | +2 | +2 | +3 | +3 | +4 |



## Other accessories and mounting systems



## Damper 49 SG

This damper consists basically of a disc and a directional grille. It is ideal for installation in "T"-pieces of duct and is compatible with any supply air terminal unit, i.e. it will not be directly connected to it.

From size 4 to 16 ( $\varnothing 100$ to 400 mm ) the damper is actuated by rotating the "worm" with a screwdriver.

From size 18 to 24 ( $\varnothing 450$ to 630 mm ) the damper is kept in position by a fixation lever.

## Mounting system SM

The mounting system SM consists of various fasteners with a ring around the diffuser neck, which press the exterior diffuser ring to the false ceiling. They are adjustable in height by means of screws, when taking off the core.

## 40.4-SF circular diffuser



## Description

40.4 SF circular diffuser with central core (2 inner rings), height adjustable by rotating.

Since the central core can be turned manually, the air can be distributed in any direction.

The diffusers are manufactured in anodised aluminium with a natural finish. The diffusers can be painted to fit different decorative needs upon request. A connection plenum can be added, enhancing air pressurisation and distribution in the diffuser.

Adjustments are made by accessing the mechanism of the damper directly from the room, with or without removing the central core.

The 40.4-SF-Q diffuser can be manufactured in a panel integrated in a modular drop ceiling panel of $595 \times 595 \mathrm{~mm}$.

## Applications

This type of diffuser is ideal for use in low and high ceilings.
The recommended installation height to supply cold and heat air, with the inner rings in lower position (no change in ring position), is 2.7 to 3.5 m .

If it is possible to change the inner ring position manually in order to switch from cooling to heating and vice versa, the recommended installation height for these diffusers is 2.7 to 6 metres. This last solu tion avoids potential problems with hot air stratification, for high installation heights.

The diffuser is easy to assemble, easy to adjust as well as great looking, making it an ideal choice for HVAC in areas such as offices, banks, schools, auditoriums, public premises, etc.

## Dimensions

See page 19.




## 40.4-SF + 49 ML

40.4-SF circular diffuser with butterfly volume control damper. Adjustments are made in the diffuser itself, removing the central rings.

## 40.4-SF + 49 MO

40.4-SF circular diffuser with butterfly volume control damper, with fin attachment to central axis. Adjustments are made in the diffuser itself, removing the central rings.

## 40.4-SF + 49 CML

40.4-SF circular diffuser with mounting shoulder for continuous ceilings. Includes butterfly volume control damper.

## 40.4-SF + PMC

40.4-SF circular diffuser with mounting bridge for sheet duct. Diffuser-bridge attachment with screws.


## 40.4-SF + PM

40.4-SF circular diffuser with mounting bridge for fibre duct. Diffuser bridge attachment with screws.

## 40.4-SF + SM

40.4-SF circular diffuser with hidden mounting system. Includes tabs, with mounting ring, adjacent to the diffuser shoulder. Heightadjustable.

Possible combinations of 40.4 SF diffusers, with volume control damper and fixing method

| 40-4SF |  | AMPERS |  |  | FIXING (METHOD) |  |  |  |  |  |  |  |  | 2 <br> 0 <br> + <br> 2 <br> 2 <br> + <br> + <br> 4 <br> 4 <br> 1 <br> 1 <br> + |  | $\begin{aligned} & \text { u } \\ & \mathbf{j} \\ & 1 \\ & \vdots \\ & \vdots \end{aligned}$ |  | 22+4411++ | 0 <br> 0 <br> 0 <br> + <br> + <br> + <br> 1 <br> 1 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| NOMINAL | 49CML | 49ML | 49MO | PLENUM | PLATE | SM | PM | PMC |  |  |  |  |  |  |  |  |  |  |  |
| 100 |  |  | \% | \% |  | * |  |  |  | * | \% |  |  |  |  | \% | * |  |  |
| 160 | \% | $\otimes$ | * | * | \% | * | * | $\otimes$ | \% | \% | * | \% | * | * | \% | * | * | \% | \% |
| 200 | * | \% | * | \% | \% | * | * | \% | * | \% | * | * | \% | * | * | \% | \% | \% | \% |
| 250 | \% | \% | * | \% | \% | \% | * | \% | \% | \% | \% | \% | \% | \% | \% | \% | * | \% | \% |
| 315 | \% | \% | * | * | * | * | \% | * | \% | * | * | \% | * | \% | \% | * | * | \% | 2 |
| 355 | \% | * | \% | * | * | \% | * | * | \% | * | * | \% | * | \% | \% | * | * | \% | \% |
| 400 | * | $\checkmark$ | \% | \% |  | * | \% | \% | \% | * | \% | \% | \% | \% | * | \% | * | \% | 2 |
| 450 |  |  | * | * |  |  |  |  |  | \% |  |  |  |  |  | * |  |  |  |
| 500 |  |  | * | * |  |  |  |  |  | * |  |  |  |  |  | * |  |  |  |
| 630 |  |  | \% | \% |  |  |  |  |  | * |  |  |  |  |  | * |  |  |  |
| 710 |  |  | \% | \% |  |  |  |  |  | * |  |  |  |  |  | \% |  |  |  |
| 800 |  |  | \% | * |  |  |  |  |  | * |  |  |  |  |  | * |  |  |  |
| 900 |  |  | $\pm$ | $\pm$ |  |  |  |  |  | * |  |  |  |  |  | * |  |  |  |

## Product codes

40.4-SFAluminium diffuser series

- $\quad$ Volume contro damper not included, unless otherwise indicated
49 ML Butterfly volume control damper
49 MO Butterfly volume control damper with attachment to central shaft
- Bridge not included, unless otherwise indicated

PM Mounting bridge for fibre duct
PMC Mounting bridge for sheet duct
SM Hidden mounting system
CML Mounting shoulder with damper
Size From 4 to 24 as per table
Ø Nom.From 100 mm to 630 mm , as per table
Q Mounted in modular drop ceiling panel of $595 \times 595$
PCFL With connection plenum
PCFL-A With insulated connection plenum
PE-45 Polystyrene plenum box for diffusers with plate of $595 \times 595 \mathrm{~mm}$

## Calculation example:

Required needs:
Air flow rate per diffuser: $300 \mathrm{~m}^{3} / \mathrm{h}$
Room height (offices): 4 m
Required pressure drop for the diffuser: below 25 Pa
Solution (see Tables 1 and 2, pages 26 and 27):
Diffuser selection: 40.4-SF-8"

- Heated supply ( $\Delta \mathrm{T}=10^{\circ} \mathrm{C}$ )
$Y_{\max }$ (maximum penetration in upper cone position): 3.2 m $\Delta \mathrm{P}_{\mathrm{t}}$ (pressure drop of the diffuser): 20 Pa , without volume control damper
Lwa = (sound power of the diffuser): $26 \mathrm{~dB}(\mathrm{~A})$, without volume control damper
- Cooled supply ( $\Delta \mathrm{T}=-10^{\circ} \mathrm{C}$ )

X (horizontal throw, with middle cone position): 2.6 m $\Delta P_{t}$ (pressure drop of the diffuser): 10 Pa , without volume control damper
Lwa = (sound power of the diffuser): $<20 \mathrm{~dB}(\mathrm{~A})$, without volume control damper

## Identification

The identification of the diffuser with the respective fitings will come coded according to the nomenclature in dicated in the adjacent table.

Coding example:
40.4-SF-8" + 49 ML + PMC
40.4-SF circular diffuser of nominal diameter 200 mm , with butterfly volume control damper and mounting bridge for sheet duct.


## Overall dimensions

### 40.4 SF diffuser

| NOMINAL | $\varnothing \mathrm{D}$ | $\varnothing \mathrm{D} 1$ | $\varnothing \mathrm{D} 2$ | $\varnothing \mathrm{D} 3$ | H | E | E 1 | F | F 1 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 100 | 99 | 100 | 187 | 225 | 75 | 18 | 8 | 13 |  |
| 160 | 159 | 160 | 245 | 291 | 86 |  |  |  |  |
| 200 | 199 | 200 | 324 | 378 | 95 | 33.5 | 14.5 | 15 | 8 |
| 250 | 249 | 250 | 390 | 454 | 104 |  |  |  |  |
| 315 | 314 | 315 | 468 | 537 | 121 |  |  |  |  |
| 355 | 354 | 355 | 545 | 624 | 134 |  |  | 29 | 9 |
| 400 | 399 | 400 | 614 | 704 | 172 |  |  | 40 | 20 |
| 450 | 449 | 450 | 689 | 788 | 187 |  |  | 50 | 25 |
| 500 | 499 | 500 | 764 | 872 | 200 | 33.5 | 14.5 | 54 | 30 |
| 630 | 629 | 630 | 955 | 1063 | 222 |  |  | 56 | 37 |
| 710 | 710 | 710 | 1070 | 1180 | 217 | 0 | 0 | 0 | 0 |
| 800 | 799 | 800 | 1200 | 1323 | 248 | 0 | 0 | 0 | 0 |
| 900 | 899 | 900 | 1350 | 1470 | 281 | 0 | 0 | 0 | 0 |



Connection plenum. Standard dimensions. 40-4-SF-PCFL


| DIFFUSER | Ø A | $\varnothing \mathrm{B}$ | $\varnothing \mathrm{C}$ | K | $\boldsymbol{\sigma} \mathrm{D}$ | H |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\mathbf{1 0 0}$ | 99 | 187 | 225 | 74,5 | 99 | 228 |
| $\mathbf{1 6 0}$ | 159 | 245 | 291 | 86 | 159 | 300 |
| $\mathbf{2 0 0}$ | 199 | 324 | 378 | 94,5 | 199 | 348 |
| $\mathbf{2 5 0}$ | 249 | 390 | 454 | 103,5 | 249 | 407 |
| $\mathbf{3 1 5}$ | 314 | 468 | 537 | 120,5 | 314 | 489 |
| $\mathbf{3 5 5}$ | 354 | 545 | 624 | 133,5 | 354 | 542 |
| $\mathbf{4 0 0}$ | 399 | 614 | 704 | 171,5 | 399 | 625 |
| $\mathbf{4 5 0}$ | 449 | 689 | 788 | 187,5 | 449 | 691 |
| $\mathbf{5 0 0}$ | 499 | 764 | 872 | 200 | 499 | 754 |
| $\mathbf{6 3 0}$ | 629 | 955 | 1063 | 222 | 629 | 906 |
| $\mathbf{7 1 0}$ | 709 | 1070 | 1180 | 217 | - | - |
| $\mathbf{8 0 0}$ | 799 | 1200 | 1323 | 248 | - | - |
| $\mathbf{9 0 0}$ | 899 | 1350 | 1470 | 281 | - | - |

Connection plenum. Standard dimensions. 40-4-SF-Q-PCFL


| DIFFUSER | ø A | ø C | K | ø D | H |
| :---: | :---: | :---: | :---: | :---: | :---: |
| $\mathbf{1 6 0}$ | 159 | 291 | 86 | 159 | 300 |
| $\mathbf{2 0 0}$ | 199 | 378 | 94,5 | 199 | 348 |
| $\mathbf{2 5 0}$ | 249 | 454 | 103,5 | 249 | 407 |
| $\mathbf{3 1 5}$ | 314 | 537 | 120,5 | 314 | 489 |
| $\mathbf{3 5 5}$ | 354 | 624 | 133,5 | 354 | 542 |

## 40.5-SF circular diffuser



## Description

40.5 SF circular diffuser with central core (2 inner rings), detachable in two positions; lower and upper, with clips.

Since the central core can be manually positioned in lower and upper position, the air can be distributed in any direction.

The diffusers are manufactured in anodised aluminium with a natural finish. The diffusers can be painted to fit different decorative needs upon request.

Adjustments are made by accessing the mechanism of the damper directly from the premises, with or without removing the central core.

This diffuser can be manufactured in a panel, using the 40.5-SF-Q model, integrated in a modular drop ceiling panel of $595 \times 595 \mathrm{~mm}$.

## Applications

This type of diffuser is ideal for use in low and high ceilings. The recommended installation height to supply cold and heat air, with the inner rings in lower position (no change in ring position), is 2.7 to 3.5 m .

If it is possible to change the inner ring position manually in order to switch from cooling to heating and vice versa, the recommended installation height for these diffusers is 2.7 to 6 metres. This last solution avoids potential problems with hot air stratification, for high installation heights.

The diffuser is easy to assemble, easy to adjust as well as great looking, making it an ideal choice for HVAC in areas such as offices, banks, schools, auditoriums, public premises, etc.

## Dimensions

See page 24.



## 40.5-SF + 49 ML

40.5-SF circular diffuser with butterfly volume control damper. Adjustments are made in the diffuser itself, removing the central rings.


## 40.5-SF + 49 MO

40.5-SF circular diffuser with butterfly volume control damper, with fin attachment to central axis. Adjustments are made in the diffuser itself, removing the central rings.


## 40.5-SF + 49 CML

40.5-SF circular diffuser with mounting shoulder for continuous ceilings. Includes butterfly volume control damper.


## 40.5-SF + PMC

40.5-SF circular diffuser with mounting bridge for sheet duct. Diffuser-bridge attachment with screws.


## 40.5-SF + PM

40.5-SF circular diffuser with mounting bridge for fibre duct. Diffuser bridge attachment with screws.

## 40.5-SF + SM

40.5-SF circular diffuser with hidden mounting system. Includes tabs, with mounting ring, adjacent to the diffuser shoulder. Heightadjustable.

Possible combinations of 40.5-SF diffusers, with volume control damper and fixing method

| $40-5 S F$ DAMPERS FIXING (N |  |  |  |  |  |  |  |  |  |  |  |  |  |  | JWd+WW6t+JSG-Ot |  |  |  | 020+40110 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| NOMINAL | 49CMK | 49MM | 49MO | PLENUM | PLATE | SM | PM | PMC |  |  |  |  |  |  |  |  |  |  |  |
| 100 |  |  | \$ | \% |  | \% |  |  |  | \% | \% |  |  |  |  | $\geqslant$ | \% |  |  |
| 160 | \% | \% | * | \% | 2 | \% | \% | Q | \% | \% | \% | \% | \% | \% | \% | \% | \% | \% | \% |
| 200 | \% | \% | \% | Q | \% | \% | Q | * | \% | \% | $\otimes$ | \% | \% | \% | \% | \% | \% | \% | \% |
| 250 | * | Q | * | Q | \% | \% | * | * | \% | \$ | * | \% | \% | \% | \% | \% | \% | \% | \% |
| 315 | \% | \% | * | * | * | \% | \% | * | \% | \% | \% | * | \% | \% | \% | \% | \% | \% | \% |
| 355 | * | * | \$ | * | \$ | \% | * | \% | \% | \$ | * | \$ | \% | \% | \% | * | \% | \% | \% |
| 400 | * | \% | * | * |  | \% | \% | * | \% | \% | \% | \% | \% | \% | \% | \% | \% | \% | * |
| 450 |  |  | * | 8 |  |  |  |  |  | \% |  |  |  |  |  | \% |  |  |  |
| 500 |  |  | * | * |  |  |  |  |  | \% |  |  |  |  |  | \% |  |  |  |
| 630 |  |  | * | * |  |  |  |  |  | * |  |  |  |  |  | * |  |  |  |

## Product codes

## 40.5-SFAluminium diffuser series

- $\quad$ Volume contro damper not included, unless otherwise indicated
49 ML Butterfly volume control damper
49 MO Butterfly volume control damper with attachment to central shaft
- $\quad$ Bridge not included, unless otherwise indicated

PM Mounting bridge for fibre duct
PMC Mounting bridge for sheet duct
SM Hidden mounting system
CMK Mounting shoulder with damper
Size From 4 to 24 as per table
Ø Nom. From 100 mm to 630 mm , as per table
Q Mounted in modular drop ceiling panel of $595 \times 595$
PCFL With connection plenum
PCFL-A With insulated connection plenum
PE-45 Polystyrene plenum box for diffusers with plate of $595 \times 595 \mathrm{~mm}$

## Calculation example:

Required needs:
Air flow rate per diffuser: $500 \mathrm{~m}^{3} / \mathrm{h}$
Room height (offices): 5 m
Required pressure drop for the diffuser: below 35 Pa
Solution (see Tables 1 and 2, pages 26 and 27):
Diffuser selection: 40.5-SF-10"

- Heated supply $\left(\Delta T=10^{\circ} \mathrm{C}\right)$
$\mathrm{Y}_{\max }$ (maximum penetration in upper cone position): 4.2 m $\Delta P_{t}$ (pressure drop of the diffuser): 29 Pa , without volume control damper
$L_{w A}=$ (sound power of the diffuser): $34 \mathrm{~dB}(\mathrm{~A})$, without volume control damper
- Cooled supply ( $\Delta \mathrm{T}=-10^{\circ} \mathrm{C}$ )

X (horizontal throw, with lower cone position): 3.5 m
$\Delta \mathrm{P}_{\mathrm{t}}$ (pressure drop of the diffuser): 12 Pa , without volume control damper
Lwa = (sound power of the diffuser): $21 \mathrm{~dB}(\mathrm{~A})$, without volume control damper

## Identification

The identification of the diffuser with the respective fitings will come coded according to the nomenclature in dicated in the adjacent table.

Coding example:

## 40.5-SF-12" + CMK

40.5-SF circular diffuser of nominal diameter 315 mm , with mounting shoulder for continuous ceilings and volume control damper.


## Overall dimensions

### 40.5 SF diffuser

| NOMINAL | $\varnothing \mathrm{D}$ | $\varnothing \mathrm{D} 1$ | $\varnothing \mathrm{D} 2$ | $\varnothing \mathrm{D} 3$ | H | E | F |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 100 | 99 | 100 | 187 | 225 | 75 | 3 | 7 |
| 160 | 159 | 160 | 245 | 291 | 86 |  |  |
| 200 | 199 | 200 | 324 | 378 | 95 | 10 | 12 |
| 250 | 249 | 250 | 390 | 454 | 104 |  |  |
| 315 | 314 | 315 | 468 | 537 | 121 |  | 24 |
| 355 | 354 | 355 | 545 | 624 | 134 |  | 30 |
| 400 | 399 | 400 | 614 | 704 | 172 | 14.5 | 35 |
| 450 | 449 | 450 | 689 | 788 | 187 | 16.5 | 41 |
| 500 | 499 | 500 | 764 | 872 | 200 | 20 | 42 |
| 630 | 629 | 630 | 955 | 1063 | 222 |  | 45 |



Connection plenum. Standard dimensions. 40-5-SF-PCFL


| DIFFUSER | $\varnothing \mathrm{A}$ | $\varnothing \mathrm{B}$ | $\varnothing \mathrm{C}$ | K | $\varnothing \mathrm{D}$ | H |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\mathbf{1 0 0}$ | 99 | 187 | 225 | 74,5 | 99 | 228 |
| $\mathbf{1 6 0}$ | 159 | 245 | 291 | 86 | 159 | 300 |
| $\mathbf{2 0 0}$ | 199 | 324 | 378 | 94,5 | 199 | 348 |
| $\mathbf{2 5 0}$ | 249 | 390 | 454 | 103,5 | 249 | 407 |
| $\mathbf{3 1 5}$ | 314 | 468 | 537 | 120,5 | 314 | 489 |
| $\mathbf{3 5 5}$ | 354 | 545 | 624 | 133,5 | 354 | 542 |
| $\mathbf{4 0 0}$ | 399 | 614 | 704 | 171,5 | 399 | 625 |
| $\mathbf{4 5 0}$ | 449 | 689 | 788 | 187,5 | 449 | 691 |
| $\mathbf{5 0 0}$ | 499 | 764 | 872 | 200 | 499 | 754 |
| $\mathbf{6 3 0}$ | 629 | 955 | 1063 | 222 | 629 | 906 |
| $\mathbf{7 1 0}$ | 709 | 1070 | 1180 | 217 | - | - |
| $\mathbf{8 0 0}$ | 799 | 1200 | 1323 | 248 | - | - |
| $\mathbf{9 0 0}$ | 899 | 1350 | 1470 | 281 | - | - |

Connection plenum. Standard dimensions. 40-5-SF-Q-PCFL


| DIFFUSER | Ø A | K | Ø D | H |
| :---: | :---: | :---: | :---: | :---: |
| $\mathbf{1 6 0}$ | 159 | 86 | 159 | 295 |
| $\mathbf{2 0 0}$ | 199 | 94,5 | 199 | 343,5 |
| $\mathbf{2 5 0}$ | 249 | 103,5 | 249 | 402,5 |
| $\mathbf{3 1 5}$ | 314 | 120,5 | 314 | 484,5 |
| $\mathbf{3 5 5}$ | 354 | 133,5 | 354 | 537,5 |

## Technical data. General considerations. Symbols

Table 1 and 3 contains the technical data on the effective velocity, throw, total pressure drop and noise level for the 40.4 SF and 40.5 SF diffuser, with the cone position in the middle position, the central core at the same height as the outer ring, achieving horizontal air discharge (air jet adjacent to the ceiling, adhering jet).

A horizontal supply is achieved, with $20 \%$ increase in throw, the same pressure drop and $4 \mathrm{~dB}(\mathrm{~A})$ less noise level, when in lower position (for the 40.4 SF diffuser), with the core of inner rings located 20 mm below the outer ring.

Table 2 and 4 contains the technical data on the effective velocity, maximum vertical penetration, total pressure drop and noise level for the 40.4 SF and 40.5 SF diffuser, with the cone position in upper position, with the core of inner rings in its top position, obtaining vertical air discharge.

## General notes

Tables 1, 2, 3 and 4

- This selection table is based on full-scale laboratory tests according to ISO 5135 and UNE-EN-ISO 3741 standards.
- To calculate the total pressure drop and total noise level of the 40.4 SF and 40.5 SF diffusers with volume control damper, refer to the respective charts for the volume control dampers.


## Table 1 and 3

- An adhering jet is used, i. e., the diffuser is mounted flush with the ceiling for horizontal air supply.
- The room height is 3 m .
- The $\Delta \mathrm{T}$ is equal to $0^{\circ} \mathrm{C}$ (difference between supply air temperature and room air temperature).
- Throws correspond to a maximum velocity in the occupied zone $(\mathrm{Vz})$ of $0.25 \mathrm{~m} / \mathrm{s}$.

Table 2 and 4

- The $\Delta \mathrm{T}$ is equal to $10^{\circ} \mathrm{C}$ (difference between supply air temperature and room air temperature)
- The maximum vertical penetration data correspond to an air jet velocity of $0 \mathrm{~m} / \mathrm{s}$.


## Symbols

$A_{K}: \quad$ Effective diffuser area, in $\mathrm{m}^{2}$
$V_{k}: \quad$ Effective velocity in $\mathrm{m} / \mathrm{s}$
$\Delta \mathrm{Pt}: \quad$ Total pressure drop (static + dynamic pressure), in Pa
Lwa-dB(A): Sound power level, in $\mathrm{dB}(\mathrm{A})$
X: $\quad$ Throw of the air jet for a maximum velocity in occupied area of $0.25 \mathrm{~m} / \mathrm{s}$, in m
$Y_{\text {max }}: \quad$ Maximum vertical throw, in $m$

## Technical data. Selection tables. 40.4 SF 40.5 SF diffusers

Table 1

| Q |  | 40-4 AND $40-5$ HORLEONIAL SERIES |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Sire | $\begin{gathered} 4^{7} \\ 0100 \end{gathered}$ | $\begin{gathered} 6^{\prime \prime} \\ 0160 \end{gathered}$ | $\begin{gathered} 8^{\prime \prime} \\ 0200 \end{gathered}$ | $\begin{gathered} 10^{2} \\ 0250 \end{gathered}$ | $\begin{gathered} 12^{\prime \prime} \\ 0315 \end{gathered}$ | $\begin{gathered} 14^{\prime \prime} \\ 0355 \end{gathered}$ | $\begin{gathered} 16^{\circ} \\ 0400 \end{gathered}$ | $\begin{gathered} 15^{\circ} \\ 0450 \end{gathered}$ | $\begin{gathered} 21^{\prime \prime} \\ 0500 \end{gathered}$ | $\begin{gathered} 24^{\prime \prime} \\ 0500 \end{gathered}$ |
| (m9/h) | (1/5) | A. $\left(\mathrm{m}^{2}\right)$ | 0.0070 | 0.0104 | 0.0187 | 0.0289 | 0.0461 | 0.0614 | 0.0734 | 0.0546 | 0.0947 | 0.1166 |
| 100 | 27.8 | $\begin{gathered} \mathrm{V}_{1}(\mathrm{~m} / \mathrm{s}) \\ \mathrm{X}(\mathrm{~m}) \\ \Delta \mathrm{P}_{1}(\mathrm{~Pa}) \\ d B(A) \end{gathered}$ | $\begin{aligned} & \hline 3.9 \\ & 1.4 \\ & 16 \\ & 27 \\ & \hline \end{aligned}$ | $\begin{gathered} 2.7 \\ 1.2 \\ 3 \\ 20 \\ \hline \end{gathered}$ | $\begin{gathered} 1.5 \\ 0.9 \\ 1 \\ \leq 20 \end{gathered}$ |  |  |  |  |  |  |  |
| 150 | 41.7 | $\begin{gathered} \mathrm{V}_{1}(\mathrm{~m} / \mathrm{s}) \\ \mathrm{X}(\mathrm{~m}) \\ \Delta \mathrm{P}_{1}(\mathrm{~Pa}) \\ d \mathrm{~B}(\mathrm{~A}) \\ \hline \end{gathered}$ | $\begin{aligned} & 5.9 \\ & 2.1 \\ & 36 \\ & 37 \\ & \hline \end{aligned}$ | $\begin{gathered} 4.0 \\ 1.7 \\ 7 \\ 24 \end{gathered}$ | $\begin{gathered} 2.2 \\ 1.3 \\ 3 \\ -20 \\ \hline \end{gathered}$ | $\begin{gathered} 1.4 \\ 1.0 \\ 1 \\ -20 \\ \hline \end{gathered}$ |  |  |  |  |  |  |
| 200 | 55.6 | $\begin{gathered} \hline V_{1}(\mathrm{~m} / \mathrm{s}) \\ \mathrm{X}(\mathrm{~m}) \\ \Delta \mathrm{P}_{1}(\mathrm{~Pa}) \\ \mathrm{dB}(\mathrm{~A}) \end{gathered}$ | $\begin{aligned} & 7.9 \\ & 2.8 \\ & 63 \\ & 45 \\ & \hline \end{aligned}$ | $\begin{aligned} & 5.3 \\ & 2.3 \\ & 13 \\ & 32 \\ & \hline \end{aligned}$ | $\begin{gathered} 3.0 \\ 1.7 \\ 5 \\ -20 \\ \hline \end{gathered}$ | $\begin{gathered} 1.9 \\ 1.4 \\ 2 \\ <20 \\ \hline \end{gathered}$ | $\begin{gathered} \hline 1.2 \\ 1.1 \\ 1 \\ 20 \\ \hline \end{gathered}$ |  |  |  |  |  |
| 300 | 83.3 | $\begin{gathered} \hline \mathrm{V}_{1}(\mathrm{~m} / \mathrm{s}) \\ \mathrm{X}(\mathrm{~m}) \\ \Delta \mathrm{P}_{1}(\mathrm{~Pa}) \\ \mathrm{dB}(\mathrm{Al}) \\ \hline \end{gathered}$ |  | $\begin{aligned} & 8.0 \\ & 3.5 \\ & 29 \\ & 43 \end{aligned}$ | $\begin{aligned} & 4.5 \\ & 2.6 \\ & 10 \\ & \leq 20 \\ & \hline \end{aligned}$ | $\begin{gathered} 2.9 \\ 2.1 \\ 4 \\ <20 \\ \hline \end{gathered}$ | $\begin{gathered} 1.8 \\ 1.7 \\ 2 \\ \hline 20 \\ \hline \end{gathered}$ |  |  |  |  |  |
| 400 | 111.1 | $\begin{gathered} \mathrm{V}_{1}(\mathrm{~m} / \mathrm{s}) \\ \mathrm{X}(\mathrm{~m}) \\ \Delta \mathrm{P}_{1}(\mathrm{~Pa}) \\ \mathrm{rm}(\mathrm{Al}) \end{gathered}$ |  | $\begin{gathered} 10.7 \\ 4.6 \\ 52 \\ 50 \\ \hline \end{gathered}$ | $\begin{aligned} & 6.0 \\ & 3.5 \\ & 18 \\ & 28 \\ & \hline \end{aligned}$ | $\begin{gathered} 3.8 \\ 2.8 \\ 7 \\ 20 \\ \hline \end{gathered}$ | $\begin{gathered} 2.4 \\ 2.2 \\ 3 \\ <20 \\ \hline \end{gathered}$ | $\begin{gathered} 1.8 \\ 1.9 \\ 2 \\ -20 \\ \hline \end{gathered}$ |  |  |  |  |
| 500 | 138.9 | $\begin{gathered} \mathrm{V}_{1}(\mathrm{~m} / \mathrm{s}) \\ \mathrm{X}(\mathrm{~m}) \\ \Delta \mathrm{P}_{1}(\mathrm{~Pa}) \\ \mathrm{dB}(\mathrm{~A}) \\ \hline \end{gathered}$ |  |  | $\begin{aligned} & 7.4 \\ & 43 \\ & 29 \\ & 34 \\ & \hline \end{aligned}$ | $\begin{aligned} & 4.8 \\ & 3.5 \\ & 12 \\ & 21 \\ & \hline \end{aligned}$ | $\begin{gathered} 3.0 \\ 28 \\ 5 \\ 5 \\ \hline 20 \end{gathered}$ | $\begin{gathered} 2.3 \\ 2.4 \\ 3 \\ -20 \\ \hline \end{gathered}$ |  |  |  |  |
| 600 | 166.7 | $\begin{gathered} \mathrm{V}_{1}(\mathrm{~m} / \mathrm{s}) \\ \mathrm{X}(\mathrm{~m}) \\ \Delta \mathrm{P}_{1}(\mathrm{~Pa}) \\ d \mathrm{~B}(\mathrm{~A}) \\ \hline \end{gathered}$ |  |  | $\begin{aligned} & 8.9 \\ & 52 \\ & 41 \\ & 39 \end{aligned}$ | $\begin{aligned} & 5.8 \\ & 4.2 \\ & 17 \\ & 26 \\ & \hline \end{aligned}$ | $\begin{array}{r} 3.6 \\ 3.3 \\ 7 \\ 20 \\ \hline \end{array}$ | $\begin{gathered} 2.7 \\ 2.9 \\ 4 \\ -20 \\ \hline \end{gathered}$ | $\begin{gathered} 2.3 \\ 2.6 \\ 3 \\ -20 \\ \hline \end{gathered}$ |  |  |  |
| 800 | 222.2 | $\begin{gathered} V_{1}(\mathrm{~m} / \mathrm{s}) \\ \mathrm{X}(\mathrm{~m}) \\ \Delta \mathrm{P}_{1}(\mathrm{~Pa}) \\ d B(\mathrm{~A}) \\ \hline \end{gathered}$ |  |  |  | $\begin{aligned} & 7.7 \\ & 5.6 \\ & 30 \\ & 34 \\ & \hline \end{aligned}$ | $\begin{aligned} & 4.8 \\ & 4.4 \\ & 12 \\ & 24 \\ & \hline \end{aligned}$ | $\begin{gathered} 3.6 \\ 3.8 \\ 7 \\ -20 \\ \hline \end{gathered}$ | $\begin{gathered} 3.0 \\ 3.5 \\ 5 \\ -20 \\ \hline \end{gathered}$ | $\begin{gathered} 2.6 \\ 3.3 \\ 3 \\ -20 \\ \hline \end{gathered}$ |  |  |
| 1000 | 277.8 | $\begin{gathered} V_{1}(\mathrm{~m} / \mathrm{s}) \\ \mathrm{X}(\mathrm{~m}) \\ \Delta \mathrm{P}_{1}(\mathrm{~Pa}) \\ d B(\mathrm{~A}) \end{gathered}$ |  |  |  | $\begin{aligned} & 9.6 \\ & 7.0 \\ & 47 \\ & 41 \end{aligned}$ | $\begin{aligned} & 6.0 \\ & 5.5 \\ & 18 \\ & 30 \\ & \hline \end{aligned}$ | $\begin{aligned} & 4.5 \\ & 4.8 \\ & 11 \\ & 22 \\ & \hline \end{aligned}$ | $\begin{gathered} 3.8 \\ 4.4 \\ 7 \\ -20 \\ \hline \end{gathered}$ | $\begin{gathered} 3.3 \\ 4.1 \\ 5 \\ <20 \\ \hline \end{gathered}$ | $\begin{gathered} 2.9 \\ 3.8 \\ 4 \\ 200 \\ \hline \end{gathered}$ |  |
| 1200 | 333.3 | $\begin{gathered} \mathrm{V}_{1}(\mathrm{~m} / \mathrm{s}) \\ \mathrm{X}(\mathrm{~m}) \\ \Delta \mathrm{P}_{1}(\mathrm{~Pa}) \\ d \mathrm{~B}(\mathrm{~A}) \\ \hline \end{gathered}$ |  |  |  |  | $\begin{aligned} & 7.2 \\ & 6.6 \\ & 26 \\ & 36 \\ & \hline \end{aligned}$ | $\begin{aligned} & 5.4 \\ & 5.7 \\ & 16 \\ & 28 \\ & \hline \end{aligned}$ | $\begin{aligned} & \hline 4.5 \\ & 5.2 \\ & 10 \\ & 21 \\ & \hline \end{aligned}$ | $\begin{gathered} 3.9 \\ 4.9 \\ 7 \\ <20 \\ \hline \end{gathered}$ | $\begin{gathered} 3.5 \\ 4.6 \\ 5 \\ -20 \\ \hline \end{gathered}$ |  |
| 1600 | 444.4 | $\begin{gathered} \mathrm{V}_{1}(\mathrm{~m} / \mathrm{s}) \\ \mathrm{X}(\mathrm{~m}) \\ \Delta \mathrm{P}_{1}(\mathrm{~Pa}) \\ d B(\mathrm{~A}) \\ \hline \end{gathered}$ |  |  |  |  | $\begin{aligned} & 9.6 \\ & 8.8 \\ & 47 \\ & 45 \\ & \hline \end{aligned}$ | $\begin{aligned} & 7.2 \\ & 7.6 \\ & 28 \\ & 37 \\ & \hline \end{aligned}$ | $\begin{aligned} & 6.1 \\ & 7.0 \\ & 19 \\ & 31 \\ & \hline \end{aligned}$ | $\begin{aligned} & 5.3 \\ & 6.5 \\ & 13 \\ & 25 \\ & \hline \end{aligned}$ | $\begin{aligned} & 4.7 \\ & 6.1 \\ & 10 \\ & 20 \\ & \hline \end{aligned}$ | $\begin{gathered} 3.8 \\ 5.5 \\ 6 \\ =20 \end{gathered}$ |
| 2000 | 535.6 | $\begin{gathered} \hline V_{1}(\mathrm{~m} / \mathrm{s}) \\ \mathrm{X}(\mathrm{~m}) \\ \Delta \mathrm{P}_{1}(\mathrm{~Pa}) \\ \mathrm{dB}(\mathrm{~A}) \\ \hline \end{gathered}$ |  |  |  |  |  | $\begin{aligned} & 9.1 \\ & 9.5 \\ & 43 \\ & 44 \\ & \hline \end{aligned}$ | $\begin{aligned} & 7.6 \\ & 8.7 \\ & 29 \\ & 38 \\ & \hline \end{aligned}$ | $\begin{aligned} & 6.6 \\ & 8.1 \\ & 20 \\ & 33 \\ & \hline \end{aligned}$ | $\begin{aligned} & \hline 5.9 \\ & 7.7 \\ & 15 \\ & 28 \\ & \hline \end{aligned}$ | $\begin{gathered} 4.8 \\ 6.9 \\ 9 \\ -20 \\ \hline \end{gathered}$ |
| 2500 | 694.4 | $\begin{gathered} \mathrm{V}_{1}(\mathrm{~m} / \mathrm{s}) \\ \mathrm{X}(\mathrm{~m}) \\ \Delta \mathrm{P}_{1}(\mathrm{~Pa}) \\ d B(\mathrm{~A}) \end{gathered}$ |  |  |  |  |  | $\begin{gathered} 11.3 \\ 11.9 \\ 67 \\ 51 \\ \hline \end{gathered}$ | $\begin{gathered} 9.5 \\ 10.9 \\ 46 \\ 45 \\ \hline \end{gathered}$ | $\begin{gathered} \hline 8.2 \\ 10.2 \\ 32 \\ 41 \\ \hline \end{gathered}$ | $\begin{aligned} & 7.3 \\ & 9.6 \\ & 24 \\ & 36 \\ & \hline \end{aligned}$ | $\begin{aligned} & \hline 6.0 \\ & 8.7 \\ & 14 \\ & 23 \\ & \hline \end{aligned}$ |
| 3000 | 833.3 | $\begin{gathered} \mathrm{V}_{1}(\mathrm{~m} / \mathrm{s}) \\ \mathrm{X}(\mathrm{~m}) \\ \Delta \mathrm{P}_{1}(\mathrm{~Pa}) \\ d \mathrm{~B}(\mathrm{~A}) \end{gathered}$ |  |  |  |  |  |  | $\begin{gathered} \hline 11.4 \\ 13.1 \\ 66 \\ 51 \\ \hline \end{gathered}$ | $\begin{gathered} \hline 9.8 \\ 12.2 \\ 46 \\ 47 \\ \hline \end{gathered}$ | $\begin{gathered} \hline 8.8 \\ 11.5 \\ 34 \\ 42 \\ \hline \end{gathered}$ | $\begin{gathered} 7.1 \\ 10.4 \\ 19 \\ 30 \\ \hline \end{gathered}$ |
| 3500 | 972.2 | $\begin{gathered} \hline \mathrm{V}_{1}(\mathrm{~m} / \mathrm{s}) \\ \mathrm{X}(\mathrm{~m}) \\ \Delta \mathrm{P}_{1}(\mathrm{~Pa}) \\ d B(\mathrm{~A}) \\ \hline \end{gathered}$ |  |  |  |  |  |  |  | $\begin{gathered} \hline 11.5 \\ 14.2 \\ 62 \\ 52 \\ \hline \end{gathered}$ | $\begin{gathered} 10.3 \\ 13.4 \\ 46 \\ 48 \\ \hline \end{gathered}$ | $\begin{gathered} \hline 8.3 \\ 12.1 \\ 26 \\ 36 \\ \hline \end{gathered}$ |
| 4000 | 1111.1 | $\begin{gathered} \mathrm{V}_{1}(\mathrm{~m} / \mathrm{s}) \\ \mathrm{X}(\mathrm{~m}) \\ \Delta \mathrm{P}_{1}(\mathrm{~Pa}) \\ d B(\mathrm{~A}) \\ \hline \end{gathered}$ |  |  |  |  |  |  |  |  | $\begin{gathered} 11.7 \\ 15.4 \\ 61 \\ 53 \\ \hline \end{gathered}$ | $\begin{gathered} 9.5 \\ 13.8 \\ 35 \\ 41 \\ \hline \end{gathered}$ |
| 5000 | 1388.9 | $\begin{gathered} \mathrm{V}_{1}(\mathrm{~m} / \mathrm{s}) \\ \mathrm{X}(\mathrm{~m}) \\ \Delta \mathrm{P}_{1}(\mathrm{~Pa}) \\ d B(\mathrm{~A}) \end{gathered}$ |  |  |  |  |  |  |  |  |  | $\begin{gathered} 11.9 \\ 17.3 \\ 54 \\ 50 \\ \hline \end{gathered}$ |

## Technical data. Selection tables. 40.4 SF 40.5 SF diffusers

Table 2

| 40-4AND 40-S VEETHCAL SELIES |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Q |  | Size | $\begin{array}{r} 4^{17} \\ 0100 \\ \hline \end{array}$ | $\begin{gathered} 6^{\prime \prime} \\ 0160 \end{gathered}$ | $\begin{gathered} 8^{\prime \prime} \\ 0200 \\ \hline \end{gathered}$ | $\begin{gathered} 10^{2} \\ 0250 \\ \hline \end{gathered}$ | $\begin{aligned} & 12^{11} \\ & 0315 \\ & \hline \end{aligned}$ | $\begin{array}{r} 14^{17} \\ 0355 \\ \hline \end{array}$ | $\begin{array}{r} 16^{\prime \prime} \\ 0400 \\ \hline \end{array}$ | $\begin{array}{r} 18^{17} \\ 0450 \\ \hline \end{array}$ | $\begin{array}{r} 21^{1 "} \\ 0500 \\ \hline \end{array}$ | $\begin{array}{r} 24^{\prime \prime} \\ 0500 \\ \hline \end{array}$ |
| $\left(\mathrm{m}^{3} / \mathrm{b}\right)$ | (1) | $\mathrm{A}_{2}\left(\mathrm{~m}^{2}\right)$ | 0.00784 | 0.0103 | 0.01493 | 0.02065 | 0.02877 | 0.04161 | 0.0571 | 0.07741 | 0.10177 | 0.18338 |
| 100 | 27.8 | $\begin{aligned} & \mathbf{V}_{\mathrm{k}}(\mathrm{~m} / \mathrm{z}) \\ & \mathbf{Y}_{\mathrm{mm}}(\mathrm{~m}) \\ & \Delta \mathrm{P}_{\mathrm{t}}(\mathrm{~Pa}) \end{aligned}$ $\mathrm{dB}(\mathrm{~A})$ | $\begin{aligned} & \hline 3.5 \\ & 1.8 \\ & 14 \\ & 36 \\ & \hline \end{aligned}$ | $\begin{gathered} 27 \\ 14 \\ 5 \\ 5 \\ \hline 20 \end{gathered}$ | $\begin{gathered} 19 \\ 11 \\ 2 \\ 2 \\ \hline 20 \end{gathered}$ |  |  |  |  |  |  |  |
| 150 | 41.7 | $\mathbf{V}_{\mathbf{k}}$ (m/s) <br> $\mathbf{Y}_{\text {man }}$ (m) <br> $\Delta \mathrm{P}_{\mathrm{t}}(\mathrm{Pa})$ | $\begin{aligned} & 5.3 \\ & 2.6 \\ & 32 \\ & 46 \\ & \hline \end{aligned}$ | $\begin{aligned} & 4.0 \\ & 21 \\ & 11 \\ & 25 \\ & \hline \end{aligned}$ | $\begin{gathered} 28 \\ 16 \\ 5 \\ -20 \\ \hline \end{gathered}$ | $\begin{gathered} 20 \\ 1.3 \\ 3 \\ -20 \\ \hline \end{gathered}$ |  |  |  |  |  |  |
| 200 | 55.6 | $\mathrm{V}_{\mathbf{k}}(\mathrm{m} / \mathrm{s})$ <br> $\mathbf{Y}_{\text {man }}$ (in) <br> $\Delta \mathrm{P}_{\mathrm{t}}(\mathrm{Pa})$ <br> $\mathrm{dB}(\mathrm{A})$ | $\begin{aligned} & 7.1 \\ & 3.5 \\ & 56 \\ & 53 \\ & \hline \end{aligned}$ | $\begin{aligned} & 5.4 \\ & 29 \\ & 19 \\ & 32 \\ & \hline \end{aligned}$ | $\begin{gathered} 3.7 \\ 22 \\ 9 \\ -20 \\ \hline \end{gathered}$ | $\begin{gathered} 27 \\ 1.7 \\ 5 \\ -20 \\ \hline \end{gathered}$ | $\begin{gathered} 19 \\ 1.3 \\ 4 \\ 20 \\ \hline \end{gathered}$ |  |  |  |  |  |
| 300 | 83.3 | $\begin{gathered} \mathbf{V}_{\mathbf{k}}(\mathrm{m} / \mathrm{s}) \\ \mathbf{Y}_{\mathrm{man}}(\mathrm{~m}) \\ \Delta \mathbf{P}_{\mathrm{t}}(\mathrm{~Pa}) \\ \mathrm{dB}(\mathrm{~A}) \\ \hline \end{gathered}$ |  | $\begin{aligned} & 81 \\ & 4.3 \\ & 43 \\ & 43 \\ & \hline \end{aligned}$ | $\begin{aligned} & 5.6 \\ & 3.2 \\ & 20 \\ & 26 \\ & \hline \end{aligned}$ | $\begin{aligned} & 4.0 \\ & 25 \\ & 10 \\ & 20 \\ & \hline \end{aligned}$ | $\begin{gathered} 29 \\ 20 \\ 9 \\ -20 \\ \hline \end{gathered}$ | $\begin{gathered} 20 \\ 1.5 \\ 7 \\ 720 \\ \hline \end{gathered}$ |  |  |  |  |
| 400 | 111.1 | $\mathrm{V}_{\mathrm{k}}(\mathrm{m} / \mathrm{s})$ <br> $\mathbf{Y}_{\text {maxin }}$ (II) $\Delta \mathrm{P}_{\mathrm{t}}(\mathrm{Pa})$ dB(A) |  | $\begin{aligned} & 10.8 \\ & 5.7 \\ & 77 \\ & 51 \\ & \hline \end{aligned}$ | $\begin{aligned} & 7.4 \\ & 4.3 \\ & 36 \\ & 34 \\ & \hline \end{aligned}$ | $\begin{aligned} & 5.4 \\ & 3.4 \\ & 18 \\ & 27 \\ & \hline \end{aligned}$ | $\begin{aligned} & 39 \\ & 26 \\ & 15 \\ & 27 \\ & \hline \end{aligned}$ | $\begin{aligned} & 27 \\ & 20 \\ & 13 \\ & 25 \\ & \hline \end{aligned}$ | $\begin{gathered} 19 \\ 16 \\ 8 \\ 22 \end{gathered}$ |  |  |  |
| 500 | 138.9 | $\begin{gathered} \mathbf{V}_{\mathbf{x}}(\mathrm{m} / \mathrm{l}) \\ \mathbf{Y}_{\operatorname{man}(\mathrm{m}}(\mathrm{m}) \\ \Delta \mathbf{P}_{i}(\mathrm{~Pa}) \\ \mathrm{dB}(\mathrm{~A}) \end{gathered}$ |  |  | $\begin{aligned} & 9.3 \\ & 5.4 \\ & 56 \\ & 40 \end{aligned}$ | $\begin{aligned} & 6.7 \\ & 4.2 \\ & 29 \\ & 34 \\ & \hline \end{aligned}$ | $\begin{aligned} & 4.8 \\ & 3.3 \\ & 24 \\ & 33 \\ & \hline \end{aligned}$ | $\begin{aligned} & 3.3 \\ & 25 \\ & 21 \\ & 31 \\ & \hline \end{aligned}$ | $\begin{aligned} & 24 \\ & 20 \\ & 12 \\ & 27 \\ & \hline \end{aligned}$ | $\begin{gathered} 1.8 \\ 1.6 \\ 7 \\ 23 \\ \hline \end{gathered}$ |  |  |
| 600 | 166.7 | $\mathrm{V}_{\mathbf{k}}(\mathrm{m} / \mathrm{s})$ <br> $\mathbf{Y}_{\text {main }}$ (II) <br> $\Delta \mathrm{P}_{\mathrm{t}}\left(\mathrm{Pa}_{\mathrm{a}}\right)$ <br> dB(A) |  |  | $\begin{array}{r} 11.2 \\ 65 \\ 80 \\ 46 \\ \hline 46 \end{array}$ | $\begin{aligned} & 81 \\ & 51 \\ & 42 \\ & 39 \\ & \hline \end{aligned}$ | $\begin{aligned} & \hline 5.8 \\ & 4.0 \\ & 35 \\ & 38 \\ & \hline \end{aligned}$ | $\begin{aligned} & 4.0 \\ & 3.0 \\ & 30 \\ & 36 \\ & \hline \end{aligned}$ | 29 24 17 32 | $\begin{aligned} & 2.2 \\ & 19 \\ & 10 \\ & 28 \\ & \hline \end{aligned}$ |  |  |
| 800 | 222.2 | $\mathrm{V}_{\mathrm{k}}(\mathrm{m} / \mathrm{s})$ <br> $\mathbf{Y}_{\text {manin}}$ (II) <br> $\Delta \mathrm{P}_{\mathrm{t}}(\mathrm{Pa})$ <br> $\mathrm{dB}(\mathrm{A})$ |  |  |  | $\begin{gathered} 10.8 \\ 6.8 \\ 74 \\ 48 \\ \hline \end{gathered}$ | $\begin{aligned} & 7.7 \\ & 5.3 \\ & 62 \\ & 46 \\ & \hline \end{aligned}$ | $\begin{aligned} & 53 \\ & 4.0 \\ & 53 \\ & 43 \\ & \hline \end{aligned}$ | $\begin{aligned} & 3 . \\ & 3.2 \\ & 31 \\ & 39 \\ & \hline \end{aligned}$ | $\begin{aligned} & 2.9 \\ & 2.5 \\ & 18 \\ & 34 \\ & \hline \end{aligned}$ | $\begin{aligned} & \hline 2.2 \\ & 2.1 \\ & 11 \\ & 29 \\ & \hline \end{aligned}$ | $\begin{gathered} 1.2 \\ 1.3 \\ 4 \\ 22 \\ \hline \end{gathered}$ |
| 1000 | 277.8 |  |  |  |  |  | $\begin{aligned} & 9.7 \\ & 6.6 \\ & 96 \\ & 53 \\ & \hline \end{aligned}$ | $\begin{aligned} & 67 \\ & 5.0 \\ & 83 \\ & 49 \\ & \hline \end{aligned}$ |  | 3.6 3.2 28 40 | $\begin{aligned} & 2.7 \\ & 2.6 \\ & 17 \\ & 34 \\ & \hline \end{aligned}$ | $\begin{gathered} \hline 1.5 \\ 1.7 \\ 6 \\ 27 \\ \hline \end{gathered}$ |
| 1200 | ${ }^{333.3}$ | $\mathrm{V}_{\mathbf{k}}\left(\mathrm{mm}^{\prime}\right.$ ) <br> $\mathbf{Y}_{\text {main }}$ (II) <br> $\Delta \mathrm{P}_{\mathrm{t}}(\mathrm{Pa})$ <br> $\mathrm{dB}(\mathrm{A})$ |  |  |  |  |  | $\begin{aligned} & \hline 8.0 \\ & 6.0 \\ & 120 \\ & 54 \\ & \hline \end{aligned}$ | $\begin{aligned} & 58 \\ & 48 \\ & 69 \\ & 50 \\ & \hline \end{aligned}$ | $\begin{aligned} & \hline 4.3 \\ & 3.8 \\ & 40 \\ & 44 \\ & \hline \end{aligned}$ | $\begin{aligned} & 3.3 \\ & 3.1 \\ & 25 \\ & 38 \\ & \hline \end{aligned}$ | $\begin{gathered} 1.8 \\ 2.0 \\ 9 \\ 30 \\ \hline \end{gathered}$ |
| 1600 | 444.4 | $\mathrm{V}_{\mathrm{k}}$ (mis) <br> $\mathbf{Y}_{\text {man }}$ (ili) $\Delta \mathrm{P}_{\mathrm{t}}(\mathrm{Pa})$ <br> $\mathrm{dB}(\mathrm{A})$ |  |  |  |  |  |  |  | $\begin{aligned} & 5,7 \\ & 5,0 \\ & 72 \\ & 72 \\ & \hline \end{aligned}$ | $\begin{aligned} & 4,4 \\ & 4,1 \\ & 44 \\ & 44 \\ & \hline \end{aligned}$ | $\begin{aligned} & 2,4 \\ & 2,6 \\ & 15 \\ & 36 \\ & \hline \end{aligned}$ |
| 2000 | 555.6 | $\begin{aligned} & \mathbf{V}_{\mathbf{V}_{\mathbf{k}}(\mathbf{m} \dot{\prime})} \\ & \mathbf{Y}_{\text {max }}(\mathbf{m}) \\ & \Delta \mathbf{P}_{t}(\mathrm{~Pa}) \end{aligned}$ $d B(A)$ |  |  |  |  |  |  |  |  | $\begin{aligned} & 5.5 \\ & 5.1 \\ & 69 \\ & 49 \end{aligned}$ | $\begin{aligned} & 3.0 \\ & 3.3 \\ & 24 \\ & 40 \\ & \hline \end{aligned}$ |
| 2500 | 694.4 | $\mathbf{V}_{\mathbf{k}}(\mathbf{m} / \mathrm{s})$ <br> $\mathbf{Y}_{\max }$ (m) $\Delta \mathrm{P}_{t}(\mathrm{~Pa})$ |  |  |  |  |  |  |  |  | $\begin{aligned} & 6.8 \\ & 6.4 \\ & 107 \\ & 54 \\ & \hline \end{aligned}$ | $\begin{aligned} & 3.8 \\ & 4.1 \\ & 37 \\ & 44 \\ & \hline \end{aligned}$ |
| 3000 | 833.3 | $d B(A)$ |  |  |  |  |  |  |  |  |  | $\begin{aligned} & \hline 4.5 \\ & 5.0 \\ & 54 \\ & 48 \\ & \hline \end{aligned}$ |
| 4000 | 1111.1 | $\begin{aligned} & \mathbf{V}_{\mathrm{k}}(\mathrm{~m} \dot{\mathrm{~m}}) \\ & \mathbf{Y}_{\max (\mathrm{m})} \\ & \Delta \mathbf{P}_{\mathrm{i}}(\mathrm{~Pa}) \end{aligned}$ dBIA |  |  |  |  |  |  |  |  |  | 6.1 6.6 96 53 |

# Technical data. Selection tables. <br> Oversized. 40.4 SF diffusers 

Table 3

| S 40-4 HORIZONTAL |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Q |  | Size | 710 | 800 | 900 |
| $\left(\mathrm{m}^{3} / \mathrm{h}\right)$ | (1/s) | $\mathrm{A}_{\mathrm{n}}\left(\mathrm{m}^{2}\right)$ | 0,3893 | 0,4951 | 0,6277 |
| 1000 | 277,8 | $\begin{gathered} \mathrm{Vn}(\mathrm{~m} / \mathrm{s}) \\ \mathrm{X}(\mathrm{~m}) \\ \mathrm{Pt}(\mathrm{~Pa}) \\ \mathrm{dB}(\mathrm{~A}) \end{gathered}$ | $\begin{gathered} 0,7 \\ 1,6 \\ 2 \\ <20 \end{gathered}$ |  |  |
| 1500 | 416,7 | $\begin{gathered} \mathrm{Vn}(\mathrm{~m} / \mathrm{s}) \\ \mathrm{X}(\mathrm{~m}) \\ \mathrm{Pt}(\mathrm{~Pa}) \\ \mathrm{dB}(\mathrm{~A}) \end{gathered}$ | $\begin{gathered} 1,1 \\ 2,4 \\ 6 \\ <20 \end{gathered}$ | $\begin{gathered} 0,8 \\ 2,2 \\ 3 \\ <20 \end{gathered}$ |  |
| 2000 | 555,6 | $\begin{gathered} \mathrm{Vn}(\mathrm{~m} / \mathrm{s}) \\ \mathrm{X}(\mathrm{~m}) \\ \mathrm{Pt}(\mathrm{~Pa}) \\ \mathrm{dB}(\mathrm{~A}) \end{gathered}$ | $\begin{gathered} 1,4 \\ 3,2 \\ 10 \\ <20 \end{gathered}$ | $\begin{gathered} 1,1 \\ 2,9 \\ 6 \\ <20 \end{gathered}$ | $\begin{gathered} 0,9 \\ 2,5 \\ 4 \\ <20 \end{gathered}$ |
| 2500 | 694,4 | $\begin{gathered} \mathrm{Vn}(\mathrm{~m} / \mathrm{s}) \\ \mathrm{X}(\mathrm{~m}) \\ \mathrm{Pt}(\mathrm{~Pa}) \\ \mathrm{dB}(\mathrm{~A}) \\ \hline \end{gathered}$ | $\begin{gathered} 1,8 \\ 4,0 \\ 15 \\ <20 \end{gathered}$ | $\begin{gathered} 1,4 \\ 3,6 \\ 10 \\ <20 \end{gathered}$ | $\begin{gathered} 1,1 \\ 3,2 \\ 6 \\ <20 \end{gathered}$ |
| 3000 | 833,3 | $\begin{gathered} \mathrm{Vn}(\mathrm{~m} / \mathrm{s}) \\ \mathrm{X}(\mathrm{~m}) \\ \mathrm{Pt}(\mathrm{~Pa}) \\ \mathrm{dB}(\mathrm{~A}) \end{gathered}$ | $\begin{aligned} & 2,1 \\ & 4,9 \\ & 22 \\ & 23 \end{aligned}$ | $\begin{gathered} 1,1 \\ 4,3 \\ 14 \\ <20 \end{gathered}$ | $\begin{gathered} 1,3 \\ 3,8 \\ 9 \\ <20 \end{gathered}$ |
| 3500 | 972,2 | $\begin{gathered} \mathrm{Vn}(\mathrm{~m} / \mathrm{s}) \\ \mathrm{X}(\mathrm{~m}) \\ \mathrm{Pt}(\mathrm{~Pa}) \\ \mathrm{dB}(\mathrm{~A}) \end{gathered}$ | $\begin{aligned} & 2,5 \\ & 5,7 \\ & 30 \\ & 28 \end{aligned}$ | $\begin{aligned} & 2,0 \\ & 5,0 \\ & 19 \\ & 22 \end{aligned}$ | $\begin{gathered} 1,5 \\ 4,5 \\ 12 \\ <20 \end{gathered}$ |
| 4000 | 1111,1 | $\begin{gathered} \mathrm{Vn}(\mathrm{~m} / \mathrm{s}) \\ \mathrm{X}(\mathrm{~m}) \\ \mathrm{Pt}(\mathrm{~Pa}) \\ \mathrm{dB}(\mathrm{~A}) \\ \hline \end{gathered}$ | $\begin{aligned} & 2,9 \\ & 6,5 \\ & 40 \\ & 31 \\ & \hline \end{aligned}$ | $\begin{aligned} & 2,2 \\ & 5,7 \\ & 24 \\ & 26 \\ & \hline \end{aligned}$ | $\begin{aligned} & 1,8 \\ & 5,1 \\ & 15 \\ & 20 \\ & \hline \end{aligned}$ |
| 4500 | 1250,0 | $\begin{gathered} \mathrm{Vn}(\mathrm{~m} / \mathrm{s}) \\ \mathrm{X}(\mathrm{~m}) \\ \mathrm{Pt}(\mathrm{~Pa}) \\ \mathrm{dB}(\mathrm{~A}) \\ \hline \end{gathered}$ | $\begin{aligned} & 3,2 \\ & 7,3 \\ & 50 \\ & 35 \end{aligned}$ | $\begin{aligned} & 2,5 \\ & 6,5 \\ & 31 \\ & 29 \\ & \hline \end{aligned}$ | $\begin{aligned} & 2,0 \\ & 5,7 \\ & 19 \\ & 23 \end{aligned}$ |
| 5000 | 1388,9 | $\begin{gathered} \mathrm{Vn}(\mathrm{~m} / \mathrm{s}) \\ \mathrm{X}(\mathrm{~m}) \\ \mathrm{Pt}(\mathrm{~Pa}) \\ \mathrm{dB}(\mathrm{~A}) \end{gathered}$ | $\begin{aligned} & 3,6 \\ & 8,1 \\ & 62 \\ & 38 \end{aligned}$ | $\begin{aligned} & 2,8 \\ & 7,2 \\ & 38 \\ & 32 \end{aligned}$ | $\begin{aligned} & 2,2 \\ & 6,4 \\ & 24 \\ & 26 \end{aligned}$ |
| 6000 | 1666,7 | $\begin{gathered} \mathrm{Vn}(\mathrm{~m} / \mathrm{s}) \\ \mathrm{X}(\mathrm{~m}) \\ \mathrm{Pt}(\mathrm{~Pa}) \\ \mathrm{dB}(\mathrm{~A}) \end{gathered}$ | $\begin{aligned} & 4,3 \\ & 9,7 \\ & 89 \\ & 43 \end{aligned}$ | $\begin{aligned} & 3,4 \\ & 8,6 \\ & 55 \\ & 37 \end{aligned}$ | $\begin{aligned} & 2,7 \\ & 7,6 \\ & 34 \\ & 31 \end{aligned}$ |
| 7000 | 1944,4 | $\begin{gathered} \mathrm{Vn}(\mathrm{~m} / \mathrm{s}) \\ \mathrm{X}(\mathrm{~m}) \\ \mathrm{Pt}(\mathrm{~Pa}) \\ \mathrm{dB}(\mathrm{~A}) \end{gathered}$ |  | $\begin{gathered} 3,9 \\ 10,0 \\ 75 \\ 41 \end{gathered}$ | $\begin{aligned} & 3,1 \\ & 8,9 \\ & 47 \\ & 35 \end{aligned}$ |
| 8000 | 2222,2 | $\begin{gathered} \mathrm{Vn}(\mathrm{~m} / \mathrm{s}) \\ \mathrm{X}(\mathrm{~m}) \\ \mathrm{Pt}(\mathrm{~Pa}) \\ \mathrm{dB}(\mathrm{~A}) \\ \hline \end{gathered}$ |  | $\begin{gathered} 4,5 \\ 11,5 \\ 98 \\ 45 \end{gathered}$ | $\begin{gathered} 3,5 \\ 10,2 \\ 61 \\ 39 \\ \hline \end{gathered}$ |
| 9000 | 2500,0 | $\begin{gathered} \mathrm{Vn}(\mathrm{~m} / \mathrm{s}) \\ \mathrm{X}(\mathrm{~m}) \\ \mathrm{Pt}(\mathrm{~Pa}) \\ \mathrm{dB}(\mathrm{~A}) \end{gathered}$ |  |  | $\begin{gathered} 4,0 \\ 11,5 \\ 77 \\ 42 \end{gathered}$ |
| 10000 | 2777,8 | $\begin{gathered} \mathrm{Vn}(\mathrm{~m} / \mathrm{s}) \\ \mathrm{X}(\mathrm{~m}) \\ \mathrm{Pt}(\mathrm{~Pa}) \\ \mathrm{dB}(\mathrm{~A}) \end{gathered}$ |  |  | $\begin{gathered} 4,4 \\ 12,7 \\ 95 \\ 45 \\ \hline \end{gathered}$ |
| 11000 | 3055,6 | $\begin{gathered} \mathrm{Vn}(\mathrm{~m} / \mathrm{s}) \\ \mathrm{X}(\mathrm{~m}) \\ \mathrm{Pt}(\mathrm{~Pa}) \\ \mathrm{dB}(\mathrm{~A}) \\ \hline \end{gathered}$ |  |  | $\begin{gathered} 4,9 \\ 14,0 \\ 115 \\ 48 \\ \hline \end{gathered}$ |
| 12000 | 3333,3 | $\begin{gathered} \mathrm{Vn}(\mathrm{~m} / \mathrm{s}) \\ \mathrm{X}(\mathrm{~m}) \\ \mathrm{Pt}(\mathrm{~Pa}) \\ \mathrm{dB}(\mathrm{~A}) \end{gathered}$ |  |  | $\begin{gathered} 5,3 \\ 15,3 \\ 137 \\ 51 \end{gathered}$ |

Table 4


## Symbols

$\mathrm{A}_{\mathrm{n}}$ :
$V_{n}$ :
$\Delta \mathrm{Pt}$ :
$\mathrm{L}_{\text {wa }}-\mathrm{dB}(\mathrm{A})$ :
X:
$Y_{\text {max }}$ :

Geometry area, in $\mathrm{m}^{2}$
Velocity in duct in $\mathrm{m} / \mathrm{s}$
Total pressure drop (static + dynamic pressure), in Pa
Sound power level, in $\mathrm{dB}(\mathrm{A})$
Throw of the air jet for a maximum velocity in occupied area of $0.25 \mathrm{~m} / \mathrm{s}$, in m
Maximum vertical throw, in $m$

## Recommendations

## 49 MM, 49 ML and 49 MO volume control dampers

The volume control dampers modify the noise level and pressure drop values expressed in the selection table. The pressure drops and sound power in $\mathrm{dB}(\mathrm{A})$ (without attenuation of the room) for the diffuser + damper combination are shown below and in the respective charts, based on the degree of damper opening.

- 49 MM and 49 ML damper (opening by degrees)


A size correction must be added to the sound power value from the chart (Ønominal dimension, in mm) according to the following table:

| $\varnothing$ | 160 | 200 | 250 | 315 | 355 | 400 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\mathrm{~dB}(\mathrm{~A})$ | -2 | 0 | +3 | +4 | +5 | +6 |

- 49 MO damper (opening by degrees)


A size correction must be added to the sound power value from the chart (Ønominal dimension, in mm) according to the following table:

| $\varnothing$ | 100 | 160 | 200 | 250 | 315 | 355 | 400 | 450 | 500 | 630 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\mathrm{~dB}(\mathrm{~A})$ | -5 | -2 | -1 | 0 | +1 | +2 | +2 | +3 | +3 | +4 |



KOOLAIR, S.L.
Calle Urano, 26
Poligono industrial $n^{\circ} 2$ - La Fuensanta 28936 Móstoles - Madrid - (España)
Tel: +34 916450033
Fax: +34 916456962
e-mail: info@koolair.com

